

# Correlation of multi-temporal ground-based images for landslide monitoring: application, potential and limitations.

Travelletti J. (1,2), Delacourt C. (3), Allemand P. (4), Malet J.-P. (1), Schmittbuhl J. (1), Toussaint R. (1), Bastard M. (1)

- (1) Institut de Physique du Globe de Strasbourg, CNRS UMR 7516, Université de Strasbourg / EOST, 5 rue René Descartes, 67084 Strasbourg Cedex, France. E-mail: julien.travelletti@unistra.fr
- (2) GEOPHEN - LETG, CNRS UMR 6554, Université de Caen Basse-Normandie, Caen, France
- (3) Institut Universitaire Européen de la Mer, CNRS UMR 6538, Université Européenne de Bretagne, Brest, France.
- (4) Laboratoire des Sciences de la Terre, CNRS UMR 5570, Université de Lyon & Ecole Normale Supérieure, Lyon, France.

## Abstract

The objective of this work is to present a low-cost methodology to monitor the displacement of continuously active landslides from ground-based optical images analyzed with a normalized Image Correlation technique. The performance of the method is evaluated on a series of images acquired on the Super-Sauze landslide (South French Alps) over the period 2008-2009. The image monitoring system consists in a high resolution optical camera installed on a concrete pillar located on a stable crest in front of the landslide and controlled by a datalogger. The data are processed with a cross-correlation algorithm applied on the full resolution images in the acquisition geometry. Then, the calculated 2D displacement field is ortho-rectified with a back projection technique using a high resolution DEM interpolated from Airborne Laser Scanning (ALS) data. The heterogeneous displacement field of the landslide is thus characterized in time and space. The performance of the technique is assessed using as reference differential GPS surveys of a series of benchmarks. The sources of error affecting the results are then discussed. The strongest limitations for the application of the technique are related to the meteorological, illumination and ground surface conditions inducing partial or complete loss of coherence among the images. Small changes in the camera orientation and the use of a mono-temporal DEM are the most important factors affecting the accuracy of the ortho-rectification of the displacement field.

Because the proposed methodology can be routinely and automatically applied, it offers promising perspectives for operational applications like, for instance, in early warning systems.

**Keywords:** image cross-correlation; image matching; landslide; time-lapse photography; displacement monitoring

## 1 Introduction

Displacement monitoring of unstable slopes is a crucial tool for the prevention of hazards. It is often the only solution for the survey and the early-warning of large landslides that cannot be stabilized or that may accelerate suddenly and potentially fluidize in highly mobile mudflows. The choice of an adequate monitoring system depends on the type and size of landslide, the range of observed velocity, the required frequency of acquisition, the desired accuracy and the financial constraints. Displacement monitoring techniques applied on landslides can be broadly subdivided in two main groups: geodetic and remote-sensing techniques.

Geodetic surveying consist in detecting geometrical changes in the landslide topography by measuring geometric parameters such as angles, distances or differences in elevation (e.g. levelling, tacheometry; Meissl & Naterop, 1995). These techniques necessitate the installation of benchmarks or targets in and outside the landslide and in measuring their position at different times. They have the advantage to be very accurate (0.2 to 2.0 cm) with a high potential of automation (Malet et al., 2002; Jaboyedoff et al., 2004; Foppe et al., 2006). Furthermore, many authors demonstrated the efficiency of permanent (Malet et al., 2002) and non-permanent (Squarzoni et al., 2005; Brunner et al., 2007) differential Global Positioning System (dGPS) for landslide monitoring with a centimetric accuracy during any daytime and weather conditions. However, because landslides can show highly variable displacement rates in time and space according to the local slope conditions (bedrock geometry, distribution of pore water pressures), the major drawbacks of the geodetic techniques are (1) to provide only discrete point measurements of the displacement and (2) the costs of installation and maintenance of the survey network. They are usually only justified in the case of a real risk for the population.

Remote-sensing techniques appear to be an interesting and complementary tool to obtain spatially-distributed information on the kinematics (Delacourt et al., 2007) which is also justified by the need to investigate landslides from safe and remote places because of the inaccessibility of mountainous terrains. Remote-sensing techniques give the possibility to discriminate stable and unstable areas and to map sectors within the landslide with different kinematics from a regional to

a local scale. They are also useful tools for a process-based analysis of the deformation field affecting the slope (Casson et al., 2005; Teza et al., 2008; Oppikofer et al., 2008). Remote-sensing techniques can be operational from spaceborne, airborne and ground-based platforms. In the last decades, the development of ground-based platforms for landslide monitoring at the local scale provided many advantages over spaceborne and airborne platforms despite a shorter spatial coverage (Corsini et al., 2006). The geometry and frequency of acquisitions are more flexible and adaptable to any type of local environment. Furthermore, the installation of the monitoring system is generally relatively easy. In addition ground-based platforms are permanent installations that allow a continuous monitoring (Casagli et al., 2004; Delacourt et al., 2007). Three main categories of ground-based remote sensing techniques are used in landslide monitoring: Ground-Based Synthetic Aperture Radar Interferometry (GB-InSAR), Terrestrial Laser Scanning (TLS) and Terrestrial Optical Photogrammetry (TOP). A non exhaustive review of the main advantages and disadvantages of these techniques is presented in Table 1. Detailed reviews of the application of GB-InSAR and TLS to landslides can be found in Luzi (2010), Corsini et al. (2006), Tarchi et al. (2003), Jaboyedoff et al. (2010), Teza et al. (2007, 2008) and Monserrat & Crosetto (2008). A state-of-the art of the application of TOP to landslide and related geomorphologic processes is given below.

TOP is a very cost-effective technique with implementation, operating and equipment costs much lower than GB-InSAR and TLS. The technique consists in acquiring digital optical images represented using a matrix of intensity values (brightness) recorded at each pixel of the Charge Coupled Device (CCD) of the camera. While aerial images are acquired on overhead photographs from an aircraft, TOP uses RGB images acquired from a spot very close to the ground (Jiang et al., 2008). In the last decades, camera self-calibration and analytical processing techniques allow the use of non-metric cameras and of simplified camera calibration algorithms to compute digital elevation models using the principle of stereoscopic views (Mikhail et al., 2001; Jiang et al., 2008). In the current state, the application of terrestrial images for landslide monitoring is mostly related to the production of DEMs for image ortho-rectification and sediment budget analysis (Bitelli et al., 2004, Pesci et al., 2004; Cardenal et al., 2008), and more recently to the characterization of the slope morpho-structure (Lim et al., 2005; Sturzenegger & Stead, 2009).

Using correlation techniques, two-dimensional displacement fields can be derived by tracking objects in two images acquired at different time. So far, image correlation techniques have been applied only on aerial and satellite images (e.g. SPOT, QuickBird, OrbView, EROS) for the creation of landslide displacement maps (Casson et al., 2003; Delacourt et al., 2004; LePrince et al., 2008); the use of image correlation on terrestrial images has not been as popular for

permanent landslide monitoring as in other application field such as in solid and fluid mechanics for the characterization of the deformation pattern of soil/rock samples (White et al., 2003; Chambon et al., 2003; Küntz et al., 2005) or for the monitoring of other natural processes such as ice glaciers (Corripio et al., 2004; Fallourd et al., 2010; Maas et al., 2008) or volcanoes (Honda & Nagai, 2002). Only Delacourt et al. (2007) demonstrated an efficient application of TOP for landslide monitoring which consisted in the determination of the landslide boundaries and in the qualitative estimation of the spatial variability of displacement at the La Clapière landslide (French Alps) with an image acquisition system installed at 1 km-distance.

Generally, the 2D displacements (in pixel) evaluated by the correlation algorithm have an accuracy of about 0.2 pixel (Casson et al., 2005; Delacourt et al., 2007) in the image plane, corresponding to an accuracy of millimeters to several centimeters for distances of about 100 m in the local coordinate system (Kraus & Waldhäusl, 1994).

The major sources of errors affecting the displacement calculations and thus potentially limiting the efficiency of TOP for an operational landslide monitoring can be classified in two groups: (i) the parameters affecting the Image Correlation computation and (ii) the external parameters influencing the ortho-rectification procedure.

The objective of this work is therefore to evaluate the potential and the limitations of TOP for the permanent monitoring of landslide using Image Correlation (IC) techniques. The dataset of images available for the Super-Sauze landslide (South French Alps) for the period 2008-2009 is used. First, the steps in the data acquisition and data processing (image correlation, ortho-rectification) are presented and the results are evaluated using the displacement of benchmark measured by DGPS. Second, the main advantages and disadvantages of the method, and the influence of external factors on the precision and the accuracy of the results are discussed. Throughout this work, the accuracy is defined as the systematic difference between a measured quantity and the true value, and precision is defined as the random difference between multiple measurements of the same quantity.

## 2 Experimental Site: the Super-Sauze landslide

To evaluate the potential of correlation of ground-based images for landslide monitoring, the dataset available at the Super-Sauze landslide, triggered in the Callovo-Oxfordian black marls of the South French Alps (Alpes-de-Haute-Provence, France; Fig. 1A, 2A, B) is used. The landslide is located in the upper part of the Sauze torrential catchment. In the 1960s, the area was affected by rock failures in the scarp area. The failed material composed of rocky panels progressively

transformed into a silty-sandy matrix integrating marly fragments of heterogeneous sizes through successive weathering cycles (Malet et al., 2003). From the 1970s until today, the landslide material is gradually filling a torrential stream located downstream with a typical range of displacement rate between 1 to 3 cm.d<sup>-1</sup> on average and possible higher velocities up to 40 cm.d<sup>-1</sup> during acceleration periods (Malet et al., 2002). In 2007, the mudslide extent over a distance of 920 m between an elevation of 1980 m at the scarp and 1760 m at the toe with an average width of 135 m and a average slope of 25°. The total volume is estimated at 560,000 m<sup>3</sup> (Travelletti & Malet, submitted).

The kinematics of the landslide is currently monitored by Differential Global Positioning System (DGPS) and Terrestrial Laser Scanning (TLS), and by a remote camera monitoring system. This instrumentation consists in a low-cost D70 Nikon non-metric reflex digital camera installed on a concrete pillar located on a stable crest in front of the landslide at a distance of 300 m from the lower part and 900 m from the main scarp (Fig. 1A, B, C). The acquisition system is controlled by a datalogger (Campbell CR10) and the power is provided by a 40 W solar panel. The characteristics of the acquisition are presented in Table 2. Each four days, four images are acquired at 11:00, 12:00, 13:00 and 14:00 GMT in order to increase the probability of having at least one image with good meteorological conditions. Each photograph (6 Mb) is stored in a native file format to avoid any loss of information.

### 3 Methodology

The steps in the data processing workflow consist in (1) correlating the images by pairs in their original acquisition geometry to prevent any loss of information, and (2) ortho-rectifying the calculated displacement fields using a high-resolution digital elevation model interpolated from airborne LiDAR data. The daily images presenting the best ground texture contrast and the most homogeneous lightening are selected based on expert judgment. The detailed methodology is summarized in Fig. 3 and described below.

#### 3.1 Principle of the Image Correlation technique

The 2D displacement field is obtained by correlating two optical images acquired at different time. The image correlation technique is based on the automatic identification of identical texture patterns within an image by maximizing a correlation function (Lewis, 1995; Baratoux et al., 2001; Debella-Gilo & Käab, 2010). Its principle adapted for landslide kinematics analysis is described in Delacourt et al. (2007). Visible ground features have to be superimposed on two

successive images on stable parts located outside the landslide. On the areas affected by landslide movements, the visible and recognizable features are shifted by the displacements. In order to quantify the ground displacements, a correlation window is defined on a reference (often the oldest) image. The corresponding window is searched in a pre-defined explored area belonging to the second image. The starting point of this explored area is the expected position of the window as if no displacement occurred between two acquisitions. The process is repeated for each pixel of the reference image. The Euclidean distance between the reference point and the matching point represents the displacement magnitudes in the image plane. By modifying the zone of interest, it is then possible to determine the displacements at various positions within the images (Fig. 4). It is important to note that the normalized cross-correlation technique cannot track objects that start to rotate significantly or are affected by important perspective distortions (Lewis, 1995).

The size of the correlation window is a compromise between the desired accuracy on the displacement estimates and the spatial resolution of the velocity field (Delacourt et al., 2007). An increase of the size of the correlation window ensures a good signal to noise ratio and thus a good precision, but the accuracy on the displacement estimates decreases because of their averaging on a larger correlation window. This compromise is difficult to find when some parts of the landslide are well defined in terms of ground texture while others parts are not. Hierarchical correlation techniques allow to overcome this problem by automatically changing the physical size of the correlation window and of the explored area during the correlation computations. The physical size is defined as the effective landslide surface covered by the correlation window (Rohaly, 2002; Aloui & Ibn-Elhaj, 2009).

In this work, a sub-pixel hierarchical correlation technique is used (Chambon, 2003; Bastard, 2009). The RGB images are first converted in gray-scale images on which a 3x3 pixel Sobel convolution matrix is applied to highlight the ground surface texture. The gradient values are then correlated (Chambon, 2003). Four successive degradations of the image resolution are applied following a pyramidal approach for changing the physical size of the correlation window and of the explored area by down-sampling the gradient values of the full resolution image (D'Antone, 1995; Kumar & Banerjee, 1998) (Fig. 4). The optimum sizes of the correlation window (16x16 pixels) and of the explored area (32x32 pixels) were identified with a trial and error procedure. These parameters are constant during the correlation computation. The correlation starts with the lowest resolution image in order to determine the largest displacements. Then the location of the pixel with the maximum cross-correlation value is used as the centre of the zone of interest for the next correlation step at a higher resolution. The spatial location of the maximum correlation value in the highest resolution image is thus progressively better estimated (Fig. 4). Ignoring high

resolution information at the first computational step decreases the probability to reach a local minima of the correlation function and, consequently, to obtain wrong matches in the correspondence solutions (Aloui & Ibn-Elhaj, 2009). In addition, this approach ensures a higher probability of reliable correlation peak detection (Anandan et al., 1993). The sub-pixel displacement is computed after the correlation at the highest resolution image. An iterative procedure is used to find the maxima of the correlation function interpolated with a bi-parabolic formula and with a maximization procedure based on the simplex method (Press et al., 1997; Chambon, 2003).

The correlation results consist in matrices of displacements  $\Delta u$  and  $\Delta v$  along the  $u$ - and  $v$ -axes in the image plane with their associated correlation index (Fig. 4). Because the pixel size is not constant in the image due to the oblique acquisition, the displacements field correlated in the image plane cannot be directly interpreted in terms of metric displacements. Therefore an ortho-rectification procedure is necessary for a quantitative analysis of the displacement fields.

### **3.2 Ortho-rectification of the displacement field using high-resolution digital elevation models (DEMs)**

The ortho-rectification procedure consists in transforming the central projection of the image into an orthogonal view of the ground by correcting the effects of various distortion sources such as camera orientation, topographic effects and lens characteristics (Kraus & Waldhäusel, 1998). In terrestrial photogrammetry, distortions induced by topography effects are the most important due to the oblique acquisition of the images. The ortho-rectification is used to convert the initial ( $u, v$ ) and the final ( $u+\Delta u, v+\Delta v$ ) positions of the displacement vectors in a local coordinate system. The conversion is possible if a Digital Elevation Model (DEM) of the object is available in order to relate two-dimensional pixel positions in the image plane to three-dimensional points in a local coordinate system using parametric approaches (Hemmler & Wiedemann, 1997).

In our approach, the rotation angles defining the external orientation of the camera are first determined using the relationship between the image coordinates ( $u, v$ ) and the local coordinates system ( $X, Y, Z$ ) given by the collinearity equations. These equations are based on the principle that each point in the local coordinate system is projected with a straight line through the projection center (origin of the camera) into the image plane (Bonneval 1972, Kraus & Waldhäusel, 1994). Knowing the exact location of the camera and assuming that the principal point coordinates is at the center of the image, the external angle defining the absolute orientation of the camera in the local reference system can be determined with Ground Control Points (GCPs; Corripio, 2004).

In our case, the GCPs located on the landslide by DGPS measurements consisted in red-yellow squared metal targets with a dimension of 0.5x0.5 m identified both in the image plane and in the local coordinate system. A serie of 95 pairs of GCPs distributed on the image plane and in the local reference system were measured (Fig. 5). The centers of the GCPs are positioned in the local coordinate system with an average 3D accuracy of 0.02 m and a standard deviation of 0.01 m. The coordinates  $(u,v)$  of the GCPs in the image plane are determined by manual picking with an estimated accuracy of about 2 pixels. Among the 95 GCPs, 45 are used to compute the external parameters and 40 are kept to calculate the accuracy of the transformation (section § 5.2.1). A least mean square minimization technique based on Singular Value Decomposition (SVD) between observed and calculated GCPs in the image plane is used to determine the external parameters that satisfy the collinearity equations (Heikkilä & Silven, 1997). Then, a backward projection method is applied to allocate a 3D coordinate to each pixel coordinate in the image plane (Mikhail et al., 2001; Corripio, 2004). In the backward projection, instead of interpolating in the local reference system, the interpolation is carried out in the image geometry. A bilinear interpolation is used to associate the  $X,Y,Z$  coordinates for each initial point  $(u,v)$  and each final point  $(u+\Delta u, v+\Delta v)$  in the image plane. Because the interpolation of the  $X,Y,Z$  coordinates is carried out directly on a regular grid, this method is easier to implement than the classical forward method which projects the image location in the DEM geometry (Mikhail et al., 2001). Moreover, a forward projection would transform the pixel coordinates in the image plane to irregularly distributed points in the local reference system which are then interpolated into a regular grid. Therefore, each point of the DEM is projected in the image using the collinearity equations. Because stereoscopic pairs of images acquired simultaneously from two cameras at different view spots are not available because of the local site configuration, two Airborne Laser Scanning (ALS) dense point clouds acquired in October 2007 and July 2009 have been used to interpolate 0.25m mesh-size DEMs with a planar and elevation accuracy of 0.07 m. The displacement correlated during the year 2008 and 2009 were orthorectified using the DEMs of 2007 and 2009 respectively. In order to avoid the projection of duplicate points in the same position, the points of the DEMs visible from the camera viewpoint are identified by using the sightline method (Fisher, 1994; Franklin & Ray, 1994). The sightline is defined as the straight line going from the camera location to the position located in the gridded DEM. The visible points of the DEM of 2009 are presented in Fig 2B. About 57 % of the landslide area is visible from the camera view point, no displacements can be obviously measured in the invisible areas. The visible points of the DEM are then back-projected and linearly interpolated in the image plane. Three grids for the X, Y and Z coordinates (Fig. 3) are then obtained. The re-projection of



the displacement vector components in the local reference system is then straightforward, and the re-projected vector components are averaged and smoothed in a regular grid with a mesh size of 1m.

The use of a mono-temporal DEM for the ortho-rectification of the displacements is a strong hypothesis that the global landslide morphology remains constant over the period and affect the accuracy of the conversion of the displacement vector in the local coordinate system. However, it will be further demonstrated that this method is still a relevant estimation for our purpose with reference to the amplitude of the observed displacements.

### 3.3 Image resolution at the terrain surface

The effective (e.g. ground) pixel size is calculated with the DEM of 2009 projected in the image geometry. The effective pixel size is one limiting parameter for the accuracy of the correlation. The pixel size depends on (1) the distance between the object and the camera (Fig. 6A) and (2) the angle of incidence which is defined as the complementary angle between the line of sight of the camera and the normal of the terrain surface (Fig. 6B). A low incidence angle means that the line of sight is nearly tangential to the topography. Consequently, the pixel projection in the local coordinate system is very close to an invisible zone from the camera view point.

The pixel size determines the minimum theoretical displacement that can be detected by the Image Correlation technique for a pixel-level correlation. Below this displacement threshold, the accuracy solely depends on accuracy of the sub-pixel correlation. Globally, the incidence angle on the landslide ranges from  $0^\circ$  to  $40^\circ$  and the pixel size varies from  $1.10^{-2} \text{ m}^2$  in the lower part (at an average distance of 300m) to  $3.10^{-2} \text{ m}^2$  in the upper part of the landslide (at an average distance of 900 m; Fig. 6A,B). The upper part is characterized with a pixel size often larger than  $0.04 \text{ m}^2$ , especially in areas where the angle of incidence is less than  $5^\circ$ . Therefore the lowest accuracy is expected in this region because a small  $\Delta v$  and  $\Delta u$  displacement can lead to an important  $\Delta X$ ,  $\Delta Y$ ,  $\Delta Z$  metric displacement.

In order to better assess the effect of the image resolution on the displacement estimate, a rigid displacement of  $\Delta v=1$  pixel and  $\Delta u=1$  pixel is imposed for each  $(u,v)$  location in the image plane and then converted in the local reference system. The metric displacements plotted versus their corresponding angle of incidence and the histograms with the cumulative distribution function of the displacements are presented in Fig. 7. If only a pixel-level correlation technique is used, the calculated displacements correspond to the minimum displacements that can be detected along the  $u$ -axis and  $v$ -axis of the image. In areas where the incidence angle is less than  $5^\circ$ , the minimum displacement drastically increases to several meters for both directions (Fig. 7A, B).

Therefore no strong confidence is given to areas whose incidence angle is lower than  $5^\circ$ . 11% and 2% of the pixels in the landslide area with an angle of incidence lower than  $5^\circ$  has a metric sensitivity to one pixel of displacement greater than 0.5 m in the  $v$ -axis and the  $u$ -axis (Fig. 7C, D). Globally, 50% of the pixels in the image plane inside the landslide area show a metric sensitivity less than 0.17 m for one pixel displacement along the  $v$ -axis and 0.07 m along the  $u$ -axis. Minimum displacements for a pixel-level correlation in respectively the  $u$  and  $v$ -direction are 0.04 m and 0.06 m in the lower part of the landslide and 0.09 m and 0.11 m in the upper part.

### 3.4 Post-processing: displacements filtering

Filtering criteria are necessary to remove the badly correlated points and improve the signal to noise ratio (Casson et al., 2003; Berthier et al., 2005; Wangenstein et al., 2006; Debella & Käab, 2010). Three criteria are used in this study to filter aberrant displacements in the image plane coordinate system and in the local coordinate system. There are based on:

1. the value of the correlation peak coefficient: loss of coherence can occur during the correlation computations because change in surface states between a reference image and the correlated image are high, resulting thus in low correlation coefficients. Defining a threshold value has the consequence to increase the percentage of realistic displacements. A high threshold coefficient of  $r=0.6$  was selected to remove the badly correlated points. However, the correlation peak coefficient alone is not a sufficient discriminating criteria because some points can display a high correlation coefficient even if they do not represent the same object (e.g. two trees or large stones having the same geometry; Casson et al., 2005);
2. the value of displacement amplitudes and directions: points which detect an upslope displacement detection and a too important displacement amplitude with reference to prior knowledge on the landslide kinematics.
3. the displacements assigned to invisible areas from the camera viewpoint because of small ortho-rectification errors in the conversion to the local coordinate system.

Table 2 presents the results of the filtering on the total number of correlated points. Displacements correlated from images acquired in the summer season (23–27 July 2008) and in the autumn season (19–23 October 2008) highlight the differences in the number of remaining values for the two seasons. The amount of remaining point after filtering varies between 80% and 90% in the summer period and can decrease to 50% in the autumn period. This is mainly explained by the different illumination conditions (low sun elevation) that affect the quality of the correlation. This aspect will be discussed further in section §6.1.3. The upper part of the landslide

is the most affected by the filtering criteria. This part generally shows a percentage of remaining values lower than in the middle and lower parts of the landslide. This is explained by the fact that the upper part has a more complex morphology. Consequently the effects of illumination changes are more important than in the middle and the lower parts, especially in autumn. In addition, the angle of incidence in this area can be low (5 to 10°) and thus sensitive to small displacements of the camera.

## 4 Results

### 4.1 Displacement maps of the landslide

A set of images over the period May–July 2008 is used to illustrate the potential of the technique for the characterization of the kinematics during an acceleration period triggered by high rainfall amounts and a fast melting of the snow cover.

Figure 8 shows an example of displacement rate (in  $\text{pixel.day}^{-1}$ ) of the ground surface in the image plane derived from image pairs of 20–28 May, 1–4 June and 9 June–13 June. The reference is the image of 20 May. The contrast in displacement rates between the landslide area and the stable area gives confidence on the calculated velocity field. One can notice that the pattern of displacement rate is heterogeneous spatially and temporarily. The upper part of the landslide displays the highest velocities ranging from 1 to 7  $\text{pixels.day}^{-1}$  while the lower part displays velocities of less than 4  $\text{pixels.day}^{-1}$ . No quantitative comparisons can be carried out at this stage because the pixel sizes vary strongly in the image (Fig. 6A). From the 20 May to the 13 June, cumulated displacements up to 110 pixels are observed in the upper part. The maximum of displacement rate is observed around the 1<sup>st</sup> June. Then the landslide decelerates to displacement rate of about 1  $\text{pixel.day}^{-1}$ .

Some local specific displacement patterns are also clearly highlighted; for instance, the presence of a stable *in-situ* crest located in the landslide body is perfectly identified in the correlated images.

Figure 9 presents the amplitude of the 3D ortho-rectified displacement rates for the period 1<sup>st</sup> June– 4<sup>th</sup> June in the local coordinate system. The difference of kinematics among the upper (until 3  $\text{m.day}^{-1}$ ) and the lower (until 1  $\text{m.day}^{-1}$ ) parts becomes more evident than in the image plane. The geometrical effect induced by the presence of the stable *in-situ* crest on the landslide kinematics is also clearly pointed out. The temporal evolution of the displacement rates is illustrated with two transversal and one longitudinal profiles on Figures 9 and 10. The difference

of displacement rates between the upper and the lower part of the landslide is particularly pointed out.

The precision of the computed displacements is assessed by performing a null hypothesis on the stable areas (Berthier et al., 2005; Casson et al., 2003). Only the points with a correlation coefficient  $r > 0.8$  are taken into account. In the image plane coordinate system, the average errors  $\mu$  range from 0.5 to 0.9 pixel with standard deviations  $\sigma$  of 0.3 to 1.2 pixel for the image pairs between the 20 May and the 25 June. In the local coordinate system, the average errors  $\mu$  range from 0.03 m to 0.11 m with standard deviations  $\sigma$  of 0.10 to 0.31 m for the image pairs between the 20 May and the 25 June.

## 4.2 Comparison with DGPS displacements

In order to estimate the accuracy and validate the calculated displacements, comparisons with independent and more accurate geodetic technique is necessary. Sixty benchmarks distributed in the stable parts and on the landslide body were monitored by DGPS with a horizontal and a vertical average accuracy of  $\pm 0.02$  m and  $\pm 0.05$  m. In total, 219 DGPS measurements are available for the period 2008–2009. In order to validate the displacements computed in the image plane, the DGPS benchmarks are projected in the image plane using the collinearity equations (Bonneval 1972, Kraus & Waldhäusel, 1998). The pixel displacements derived from the image correlation are then averaged in a perimeter of 16 pixels around each benchmark. The results are presented in Figure 11A. A correlation coefficient of  $r=0.98$  is found between DGPS measurements and Image Correlation, and an average relative accuracy of 11% is determined (Fig. 11C). In order to validate the metric displacements in the local coordinate system, the ortho-rectified displacements are averaged in an area of  $4 \text{ m}^2$  around each benchmark and compared with the DGPS displacements. A correlation coefficient of  $r=0.95$  is found (Fig. 11B), and an average relative accuracy of 20% is determined (Fig. 11D).

## 5 Discussion: sources of errors

The major sources of errors affecting the displacement calculations and thus potentially limiting the efficiency of the TOP for an operational landslide monitoring are the parameters affecting the Image Correlation computation and the external parameters influencing the ortho-rectification procedure.

## 5.1 Sources of errors affecting the Image Correlation computation

### 5.1.1 Accuracy and precision of the Image Correlation algorithm

One limitation of the Image Correlation technique is directly linked to the correlation algorithm used for matching the image pairs and to the sub-pixel interpolation method (Debella-Gilo & Kääb, 2010). The performance of a measurement system can be assessed by considering the errors associated in terms of accuracy and precision. In this section, the accuracy is represented by the average misfit between the measurements and the true value. Precision is represented by the standard deviation of the misfit between the measurements and the true value.

A series of experimental tests were carried out to assess the precision of the Image Correlation technique. The series of tests allow to investigate the influences of the size of the correlation window and of the level of noise observed in the images. Homogeneous imposed displacements (systematically equal to a multiple of pixels to avoid image resampling; Chambon & Schmittbuhl, 2003) are applied to pairs of images to create synthetic images. Furthermore, three levels of Gaussian noise were added to the original images with a mean noise level imposed to zero and variances  $\sigma^2$  imposed to  $10^{-4}$ ,  $10^{-3}$  and  $10^{-2}$  (Fig. 12A). Then the Image Correlation technique is applied on the original image taken as reference and on the synthetic image with different sizes of correlation windows (5, 10, 16, 20, 30 and 50 pixels). For each correlation window, fifteen imposed displacements were realized with an amplitude ranging from 1 to 23 pixels along the  $u$  and  $v$ -directions. The analysis was conducted by comparing the noisy synthetic images with the reference image. In the optimal case, the measured displacement would be identical to the imposed displacement.

Each Image Correlation analysis revealed displacement differences distributed close to zero (mean accuracy of  $5.10^{-4}$  pixels). As observed by Hild et al. (2003), the precision of the correlation algorithm mainly depends on the pixel fraction of the displacement. Larger correlation windows produce less scattered displacements and therefore improve the precision. By plotting the standard deviation of the calculated displacements against the size of the correlation window, the influence of the correlation window size can be pointed out (Fig. 12B). For very low level of noise, the precision is less than 0.1 pixel for a size of correlation window greater than 5x5 pixels. For higher level of noise, the precision is more dependent on the size of the correlation window. Because homogenous displacements field were imposed in the image, the accuracy (average misfit) is similar for small and large correlation windows. In reality, the displacement field becomes more heterogeneous at higher resolution. Therefore, an increase of the size of the

correlation window implies a decrease of the displacement accuracy, but, as shown in these tests, an increase of the precision.

### **5.1.2 Influence of ground surface state**

The time lag between two image acquisitions is one of the critical factors that affect the correlation computation. This time has to be long enough to increase the signal (e.g. landslide displacement) but short enough to preserve the tracked features (Berthier et al., 2005). Loading of the snowpack on the ground during Winter, surface erosion due to fast snow melting and the development of water-saturated ponds in Spring, weathering of the objects, growing of grass and large deformations are environmental processes that significantly modify the surface state during a year. Such correlation errors are characterized by very low correlation coefficients, very large displacement amplitudes or randomly-distributed displacement directions in comparison to the neighbor pixels (Fig. 13). On average, about 20 to 25% of the points are usable from one year to the next year (using a correlation window of 16\*16 pixels and with a correlation coefficient threshold of 0.8). Consequently, the construction of long time series of displacements with the image correlation technique is a difficult task for the site. The range of cumulated displacement rates observed over a period of 16 months (May 2008–September 2009) is illustrated by tracking the displacement at three locations in the upper (pt 1), middle (pt 2) and lower (pt 3) parts of the landslide at the direct vicinity of benchmark measured by DGPS (Figs. 9, 11). In our case, the cumulated displacements of the year 2009 are adjusted on those of 2008 using GCPs measured with DGPS at the vicinity of the points pt1, pt2 and pt3. The monitoring of a few benchmark with geodetic techniques is therefore necessary to combine displacement pattern observed in image pairs acquired over the period May 2008–September 2009 (74 pairs of images). After the acceleration period of Spring 2008, the displacement rates are decreasing to relative constant values of about 0.02 m.day<sup>-1</sup> in the lower and middle parts and 0.05 m.day<sup>-1</sup> in the upper part computed over the period July to October (Fig 14). Although these displacement rates are very close to the resolution of the image, the calculated displacements are in very good agreement with the displacement of the benchmarks measured by DGPS, demonstrating that the Image Correlation technique is an efficient technique to complement on-site measurements.

### **5.1.3 Influence of illumination conditions**

The difference observed in RGB intensities in various images acquired with various solar illumination angles is an important limited factor essentially in terms of changes of the shadow

areas (Berthier et al., 2005). In order to assess the influence of illumination conditions on the image correlation results, two experiments are carried out.

The first experiment consists in correlating images acquired at different times within a day. Four photographs acquired 11:00, 12:00, 13:00 and 14:00 GMT in a period of small displacements (August 2009) and of clear sky conditions are correlated. The results indicate that illumination changes can lead to an average and a standard deviation of pixel-level error of respectively  $\mu_{1h}=1.31$  and  $\sigma_{1h}=0.03$ ,  $\mu_{2h}=1.35$  and  $\sigma_{2h}=0.12$ ,  $\mu_{3h}=1.89$  and  $\sigma_{3h}=0.18$  pixel for time-interval acquisition of respectively 1, 2 and 3 hours. The results demonstrate that the correlation of images acquired in nearly similar illumination conditions can display a pixel-level precision.

The effect of illumination changes can be larger if the images are acquired at different seasons. This influence cannot be assessed by correlating images distant in time because of the landslide displacements. Therefore the second experiment consists in creating synthetic images with different shadow areas as a function of the sun azimuth and elevation (Burrough & McDonell, 1988). Only the shadows created by direct solar illumination are analyzed assuming clear-sky conditions; the effects of reflected and diffuse illuminations are neglected. First, the shaded relief on the landslide is computed from the DEM in the local coordinate system. Then, the shaded relief is projected and linearly interpolated in the image plane coordinate system. 97 shaded relief images were created with different artificial illuminations. An example of shaded relief image is represented in Figure 5. Because a preference is given to correlate images taken when the sun elevation is maximal (Delacourt et al., 2007), a shaded relief image with a sun elevation of  $65^\circ$  and a sun azimuth of  $250^\circ$  (illumination coming from the South-West) is chosen as the reference image for the correlation. It represents the illumination conditions on the landslide in the month of July at 12:00 GMT in clear sky conditions. The reference image is correlated with the shaded relief images, and the calculated displacements are compared to the errors induced by illumination changes. The mean displacement error and the mean correlation coefficient are used to characterize the influence of illumination changes on the image. Because only the shadow intensities are correlated, the errors are overestimated and are therefore represented by a normalized index.

As expected, the correlation of the synthetic images show that the correlation coefficient tends rapidly to  $r=1$  when the sun elevation is closer to the reference image (at 12.00 GMT) and the slope of the relationship depends on the sun azimuth (Fig. 15A). At the opposite, the correlation coefficient drops quickly when the illumination comes from the South-East (azimuth of  $120^\circ$ ) and shows a strong sensitivity to sun elevation changes. Low sun azimuth ( $120^\circ$ ) and low elevation angles ( $30^\circ$ ) typically represent illumination conditions at the end of the daytime which are thus

not optimal for the correlation. In addition, low sun elevations ( $30^\circ$ ) and higher azimuths ( $200^\circ$ ) are typical illumination conditions of the autumn period at 12.00 GMT. These images are also not very relevant for the calculation of the displacements because the correlation coefficient is low. This finding is in agreement with Table 2 which indicates the amount of interpretable displacements is lower in the autumn season than in the summer season (lower correlation coefficients).

Figure 15B presents the mean correlation coefficient versus the displacement noise index. As expected, for sun azimuths equal to the reference image ( $240^\circ$ ), the displacement noise decreases with an increase of the correlation coefficient. In very bad illumination conditions (e.g. a low sun elevation and a sun azimuth opposite to the reference  $-100^\circ$ ), the trend is inversed because the image becomes very low textured (most areas of the landslide are in the shadow with homogeneous intensity values). In that case, no maximum correlation value is computed, resulting in a null displacement with the correlation algorithm used in this study. Similar results are observed for images displaying homogeneous texture such as for instance in backlighting conditions, in foggy meteorological conditions or when the ground surface is covered by snow. Therefore, correlation of images with a too important time-lapse has to be avoided to minimize illumination effects. A possible alternative is to correlate images under diffused illumination (cloudy day) thus providing a more homogenous lightning. At the opposite, correlation of images acquired at the same solar time in the day and when the sun elevation is maximal is optimal.

## **5.2 Sources of errors affecting the ortho-rectification procedure**

### **5.2.1 Influence of camera orientation**

The accuracy camera orientation is a parameter affecting both the image geometry and the accuracy of the geo-referencing (Mikhail et al., 2001). If changes in external orientations of the camera are small, the image geometry is not significantly affected. Consequently a homogeneous component in the correlated displacement field is visible in the image plane (Fig. 16A). This misfit can be significant in the areas where the expected displacements are low or null such as in the stable parts. This systematic error can be corrected assuming a rigid translation of the image by removing the average  $\Delta u$  and  $\Delta v$  misfits (observed on the stable parts of the images such as stable crests or on reference targets located outside the landslide; Fig. 2B, A; Fallourt et al., 2010). Nevertheless this correction is not fully optimal, because the geometric deformations caused by the slight orientation changes of the camera depend on the object distance. Therefore,



after correction of the homogeneous component in the image plane, an average residual misfit of about 0 to 2 pixels is observed .

In order to evaluate the accuracy of the external orientation that influences the georeferencing quality, fourty GCPs not introduced in the minimization processes of section §3.2.3 are used. The shift between the projected and the observed GCPs positions in the image plane is thus determined (Fig. 16B). A mean shift error of, respectively, -0.20 and -0.08 pixel with a standard deviation of 1.59 and 1.51 pixels in the  $u$  and  $v$ -directions respectively is obtained (Table 4). The accuracy of the external parameters in the georeferencing procedure in the local coordinate system is calculated by comparing the back-projected GCPs identified in the image plane with the GCPs positions measured with DGPS and located in the stable parts. The absolute accuracy in  $X$ ,  $Y$  and  $Z$  coordinates are presented in Table 4. Because most of GCPs in the stable parts are located in the background of the image (750 m from the camera location) where the ground pixel size is about 20 cm, the mean 3D error (0.14 m) and the standard deviation (0.56 m) of the positioning are not representative of the areas of the landslide located closer to the camera (300 m). Nevertheless, because the standard deviation of the GCP located in the image plane are close to the accuracy of the GCPs picking, the determination of the camera orientation is considered acceptable. Furthermore, the good coherence between the shaded relief images (Fig. 5) and the true images (Fig. 2A) shows that the quality of the determination of the camera orientation is satisfying.

### 5.2.2 Influence of the DEM

The accuracy of the DEM used in the ortho-rectification procedure is important to correct large distortion induced by the topography, which in turn controls the accuracy of the displacements in the local coordinate system. Therefore, the actual necessity of using a mono-temporal DEM for the complete series of image pairs has to be addressed. In order to evaluate its influence on the ortho-rectified displacements, the displacements of the 1<sup>st</sup> June–4<sup>th</sup> June 2008 originally ortho-rectified with the DEM of October 2007 (Fig. 9) are compared with those orthorectified with the DEM of July 2009 documenting a slightly different landslide morphology (Fig. 17A, B). The observed differences in displacement are presented relative to the displacement orthorectified with the DEM of 2007. The differences vary spatially in the landslide area. Despite some areas displaying differences in displacement larger than 75%, the average difference is 21% which is very similar to the differences observed with the DGPS measurements (Fig. 11D). As a consequence, the influence of the DEM on the accuracy of the displacement is more important than the influence of the camera orientation, the image resolution and changes in illumination

conditions. For large displacements, morphologic changes become significant and the errors on the displacements increase. The computation of multi-temporal DEMs for each image is therefore a pre-requisite to improve the accuracy of the ortho-rectified displacements. Nevertheless, in case of a translational landslide characterized by low changes in elevation, the use of the same DEM constitutes still an acceptable 1<sup>st</sup>-order estimate.

## 6 Conclusion

The potential of multi-temporal correlation of ground-based images for landslide monitoring has been assessed using the dataset available on the Super Sauze landslide (South French Alps). A methodology to compute displacement rates both in the image plane coordinate system and in the local coordinate system has been proposed.

The results demonstrated clearly the potential and the limitation of this technique by identifying the heterogeneous displacement field, in space and in time, of the landslide. The camera monitoring allowed to characterize displacements up to 3 m.day<sup>-1</sup> during an acceleration period, and displacement of about 0.02 m.day<sup>-1</sup> computed over the period July to September (the less active period). The results are in good agreement with previous knowledge on the landslide kinematics and are in very good agreement with benchmark displacements measured by DGPS.

For objects located in a range of 300 to 900 m from the camera location, this study showed that the pixel size can vary from 0.005 to 0.04 m<sup>2</sup> according to the resolution of the image (2000x3008 pixels) and the angle of incidence of the line of sight. The orientation of the line of sight (depending on the location and orientation of the camera) to the ground surface has to be considered before installing a permanent monitoring system. Areas of low incidence angles (< 5°) are very sensitive to small movements of the camera. Therefore, the angle should be the most perpendicular as possible to the mean displacement vector of the landslide. 3D displacements of less than 0.04 m and 0.06 m in the lower part of the landslide and 0.09 m and 0.11 m in the *u* and *v*-directions are difficult to measure over a period of four days without a sub-pixel correlation algorithm.

The strongest limitations are independent of the acquisition system and are related to the meteorological and illumination conditions and the ground surface changes inducing partial or complete loss of coherence between pairs of images. During the winter season (from November to May), the presence of snow impedes reliable correlation results and excessive ground deformations between two consecutive years impede valid displacement measurements even if the images are acquired during the same solar time. The small changes in the camera orientation

and the use of a constant DEM are the most important parameters that affect the accuracy of the ortho-rectification of the displacement field. A regular acquisition of multi-temporal DEMs through airborne or terrestrial laser scanning or stereoscopic photogrammetric views is believed to be a priority to significantly improve the accuracy of the technique. The errors induced by the sub-pixel correlation algorithm are thus insignificant compared to the influences of the other parameters cited previously.

The results demonstrate that Image Correlation techniques implemented in permanent monitoring system is particularly interesting for monitoring landslides characterized by annual pluri-decimetric displacements. In addition, this low cost technique is a very suitable alternative for inaccessible landslides or areas without access to power supply. Furthermore, because the proposed methodology does not require GCPs except for determining the external orientation of the camera and for combining displacement pattern observed in image pairs acquired over two years, the methodology can be routinely and automatically applied to new pairs of images. Therefore this study offers very promising perspectives for operational applications which can be potentially integrated in an early warning system by considering additional efforts in direct data transmission. Finally, inversion of the displacement field could be developed to characterize the macroscopic rheological properties of the landslide material.

## Acknowledgements

This work was supported by the European Commission within the Marie Curie Research and Training Network '*Mountain Risks: from prediction to management and governance*' (2007-2010, Contract MCRTN-035798) and by the FP7 Large-scale Integrating Project '*Safeland: Living with landslide risk in Europe*' (2009-2012, Contract 226479). The ortho-images and the airborne LiDAR data of the Super-Sauze landslide have been acquired by the Helimap System service in 2009. The authors would like to acknowledge André Stumpf (University of Strasbourg, France & University of Twente, Netherlands) and Sabrina Rothmund (University of Stuttgart, Germany) for their help in the field. Special thanks are also due to Bas van Dam (Utrecht University, Netherlands) who designed the automatic monitoring system.

## References

- 1
- 2
- 3 618 Alaoui El. M. I., & Ibn-Elhaj E. (2009). A robust hierarchical motion estimation algorithm in
- 4 619 noisy image sequences in the bispectrum domain. *Signal Image and Video Processing*, 3,
- 5 620 291-302.
- 6
- 7 621 Anandan, P., Bergen, R.J., Hanna, K.J., & Hanna, K.J. (1993). Hierarchical model-based motion
- 8 622 estimation. In L. Sezan, (Eds.), *Image Sequence Analysis*. Kluwer, Dordrecht.
- 9
- 10 623 Antonello, G., Casagli, N., Farina, P., Leva, D., Nico, G., Sieber, A.J., & Tarchi, D. (2004).
- 11 624 Ground-based SAR interferometry for monitoring mass movements. *Landslides*, 1, 21-28.
- 12
- 13 625 Baratoux, D., Delacourt, C., & Allemand, P. (2001). High-resolution digital elevation models
- 14 626 derived from Viking Orbiter images: Method and comparison with Mars Orbiter Laser
- 15 627 Altimeter Data. *Journal of Geophysical Research*, 106, 32927-32941.
- 16
- 17 628 Bastard M., (2009). Caractérisation de la cinématique de glissement de terrain par technique de
- 18 629 correlation d'image optique. Master thesis. University of Strasbourg (EOST). Institut de
- 19 630 Physique du Globe, Strasbourg, France.
- 20
- 21 631 Berthier, E, Vadon, H., Baratoux, D., Arnaud, Y., Vincent, C., Feigl, K. L., Rémy, F., & Legrésy
- 22 632 B. (2005). Surface motion of mountain glaciers derived from satellite optical imagery.
- 23 633 *Remote Sensing of Environment*, 95, 14-28.
- 24
- 25 634 Besl, P., & McKay, N. (1992). A method for registration of 3-D shapes. *IEEE Transactions on*
- 26 635 *Pattern And Machine Intelligence*, 14, 239-256.
- 27
- 28 636 Bitelli G., Dubbini M., & Zanutta A. (2004). Terrestrial laser scanning and digital
- 29 637 photogrammetry techniques to monitor landslides bodies, *International Archives of*
- 30 638 *Photogrammetry, Remote Sensing and Spatial Information Sciences* 35, 246–251.
- 31
- 32 639 Bonneval, H., (1972). Levés topographiques par photogrammétrie aérienne. In Eyrolles (Eds.),
- 33 640 *Photogrammétrie générale: Tome 3, Collection scientifique de l'Institut Géographique*
- 34 641 *National*, Paris, France.
- 35
- 36 642 Brunner, F., Macheiner, K., & Woschitz, H. (2007). Monitoring of deep-seated mass movements.
- 37 643 *Proceedings of the 3rd International Conference on Structural Health Monitoring of*
- 38 644 *Intelligent Infra-structure*, Vancouver, Canada.
- 39
- 40 645 Burrough, P. A., & McDonell, R.A. (1998). *Principles of Geographical Information Systems*
- 41 646 ,Oxford University Press, New York.
- 42
- 43 647 Casagli, N., Farina, P., Leva, D., & Tarchi, D. (2004). Application of ground-based radar
- 44 648 interferome-try to monitor an active rock slide and implications on the emergency
- 45 649 management. In E. Kluwer (Eds.), *The NATO Advanced Research Workshop*, Celano, Italy.
- 46
- 47 650 Casson, B., Baratoux, D., Delacourt, D., & Allemand, P. (2003). “La Clapière” landslide motion
- 48 651 observed from aerial differential high resolution DEM. *Engineering. Geology*, 68, 123-139.
- 49
- 50
- 51
- 52
- 53
- 54
- 55
- 56
- 57
- 58
- 59
- 60
- 61
- 62
- 63
- 64
- 65

- 652 Casson B., Delacourt C., & Allemand, P. (2005). Contribution of multi-temporal sensing images  
653 to characterize landslide slip surface – Application to the La Clapière Landslide (France).  
654 *Natural Hazards and Earth System Sciences*, 5, 425-437.
- 655 Cardenal, J., Mata, E., Perez-Garcia, J.L., Delgado, J., Andez, M.A., Gonzalez, A., Diaz-de-  
656 Teran, J.R. (2008). Close Range Digital Photogrammetry Techniques applied to Landslide  
657 Monitoring. International Archives of the Photogrammetry, *Remote sensing and Spatial*  
658 *Information Sciences*. Vol XXXVII. Part B8.
- 659 Chambon G. (2003). Caractérisation expérimentale du frottement effectif des zones de faille. PhD  
660 Thesis. Université Paris XI Orsay, ENPC..
- 661 Chambon, G., & Schmittbuhl, J. (2003). Shear with comminution of a granular material:  
662 Microscopic deformations outside the shear band. *Physical Review E*, 68, 1-8.
- 663 Corripio, J.G. (2004). Snow surface albedo estimations using terrestrial photography.  
664 *International Journal of Remote Sensing*, 25(24), 5705-5729.
- 665 Corsini, A., Farina P., Antonello G., Barbieri M., Casagli N., Coren F., Guerri L., Ronchetti F.,  
666 Sterzai P., & Tarchi D. (2006). Space-borne and ground-based SAR interferometry as tools  
667 for landslide hazard management in civil protection. *International Journal of Remote*  
668 *Sensing*, 27, 2351 - 2369.
- 669 D’Antone, I. (1995). Hierarchical correlation for track finding. *Nuclear Instrument and Methods*  
670 *in Physics Research*, 356, 476-484.
- 671 Debella-Gilo M., & Kääb A. Sub-pixel precision image matching for measuring surface  
672 displacements on mass movements using normalized cross-correlation. *Remote Sensing of*  
673 *Environment* (2010).
- 674 Delacourt, C., Allemand P., Casson B., & Vadon H. (2004). Velocity field of the “La Clapiere”  
675 landslide measured by the correlation of aerial and Quick-Bird satellite images. *Geophysical.*  
676 *Research Letters*, 31, 1-5.
- 677 Delacourt, C., Allemand, P., Berthier, E., Raucoules, D., Casson, B., Grandjean, P., Pambrun, C.,  
678 & Varel, E. 2007. Remote-sensing techniques for analysing landslide kinematics: a review.  
679 *Bulletin de Société Géologique*, 178, 89-100.
- 680 Fallourd, R., Vernier, F., Friedt J.-M., Martin, G., trouvé, E., Moreau, L. & Nicolas, J.-M. (2010).  
681 Monitoring temperate glacier with high resolution automated digital cameras – Application to  
682 the Argentière Glacier. in: Paparoditis N., Pierrot-Deseilligny M., Mallet C. & Tournaire O.  
683 (Eds.), IAPRS, Vol. XXXVIII, Part 3B, Saint-Mandé, France., 1-23.
- 684 Fisher, P.F. (1991). First experiments in viewshed uncertainty: The accuracy of the viewshed  
685 area. *Photogrammetric Engineering Remote Sensing*, 57, 1321-1327.

- 686 Foppe, K., Barth, W., & Preis, S. (2006). Autonomous Permanent Automatic Monitoring System  
687 with Robot-Tacheometers. *Proceedings of the XXIII International FIG Congress*, Munich,  
688 Germany.
- 689 Franklin, W.R., & C.K. Rav. (1994). Higher isn't necessarily better: Visibility algorithms and  
690 experiments, *Proceedings of the 6<sup>th</sup> International Symposium on Spatial Data Handling*,  
691 Edinburgh, Scotland, 2, 751-770.
- 692 Heikkila, J., & Silven, O. (1997). A four-step camera calibration procedure with implicit image  
693 correction. *IEEE Computer. Society*, 1106-1112.
- 694 Hemmleb, M., & Wiedemann, A. (1997). Digital Rectification and Generation of Orthoimages in  
695 Architectural Photogrammetry. *CIPA International Symposium*, IAPRS, XXXII, Part 5C1B  
696 (pp. 261-267), Göteborg, Sweden.
- 697 Hild F. (2003). Mesure de champs de déplacement par corrélation d'images et applications en  
698 mécanique des solides. *Notes de cours IPSI*. Laboratoire de Mécanique et Technologie,  
699 CNRS-UMR 8535, Université Paris 6, France.
- 700 Honda, K., & M. Nagai (2002), Real-time volcano activity mapping using ground-based digital  
701 imagery, *ISPRS Journal of Photogrammetry and Remote Sensing*, 57, 1-2, 159-168.
- 702 Jaboyedoff M., Ornstein P., & Rouiller J.-D. (2004). Design of a geodetic database and associated  
703 tools for monitoring rock-slope movements: the example of the top of Randa rockfall scar.  
704 *Natural Hazards and Earth System Science*, 4, 187-196.
- 705 Jaboyedoff, M., Oppikofer T., Abellan A., Derron M.-H., Loye A., Metzger R., & Pedrazzini A.  
706 (2010). Use of LiDAR in landslide investigations: a review. *Natural Hazards*. doi  
707 10.1007/s11069-010-9634-2
- 708 Jiang, R., Jauregui, D.V., & White, K. (2008). Close-range photogrammetry applications in  
709 bridge measurement: Literature review. *Measurement*, 41, 823-834.
- 710 Kraus, K. & Waldhäusl, P., (1994). *Photogrammetry, Fundamentals and Standard processes*. vol  
711 1. Hermès (editor), Paris.
- 712 Kumar, S., & Banerjee, S., (1998). Development and application of a hierarchical system for  
713 digital particle image velocimetry to free-surface turbulence. *Physics of Fluids*, 10, 160-177.
- 714 Küntz, M., Jolin, M., Bastien, J., Perez F., & Hild, F. (2007). Digital image correlation analysis of  
715 cracks behavior in a reinforced concrete beam during a load test. *Canadian journal of civil  
716 engineering*, 33, 1418-1425.
- 717 LePrince, S., Berthier, E., Ayoub, F., Delacourt, C., & Avouac, J.- P. (2008). Monitoring Earth  
718 Surface Dynamics With Optical Imagery. *Eos*, 89, 1-5.
- 719 Lewis, J.P., (1995). Fast normalized cross-correlation. *Vision Interface*, 120-123.

- 720 Lim, M., Petley, D.N., Rosser, N.J., Allison, R.J., Long, A.J. & Pybus, D. (2005). Combined  
721 digital photogrammetry and time-of-flight laser scanning for monitoring cliff evolution. *The*  
722 *Photogrammetric Record*, 20, 109-129.
- 723 Luzi, G., (2010). Ground based SAR interferometry: a novel tool for Geoscience. In:  
724 Geoscience and Remote Sensing, New Achievements, P.Imperatore & D. Riccio (Editors),  
725 ISBN: 978-953-7619-97-8. In print.
- 726 Malet, J.-P., Maquaire, O., & Calais, E. (2002). The use of global positioning system techniques  
727 for the continuous monitoring of landslides. *Geomorphology*, 43, 33-54.
- 728 Malet, J.-P. (2003). Les glissements de type écoulement dans les marnes noires des Alpes du Sud.  
729 Morphologie, fonctionnement et modélisation hydromécanique. PhD Thesis in Earth  
730 Sciences, Université Louis Pasteur, Strasbourg.
- 731 Mantovani, F. Soeters R., & van Western C.J. (1996). Remote sensing techniques for landslide  
732 studies and hazard zonation in Europe. *Geomorphology*, 15, 213-225.
- 733 Maas, H.-G., Schwalbe, E., Dietrich, R., Bäessler, M., & Ewert, H. (2008). Determination of  
734 spatio-temporal velocity fields on glaciers in West- Greenland by terrestrial image sequence  
735 analysis. *IAPRS*, XXXVII, Part B8 Beijing, China, 1419-1424.
- 736 Meissl, A., & Naterop, D. (1995). Automatic Measuring System for Permanent Monitoring –  
737 Solexperts GeoMonitor. *Proceedings of Field Measurements in Geomechanics 4th*  
738 *International Symposium*, Bergamo, Italy, 489-494.
- 739 Mikhail, E., Bethel, J. S., & McGlone, J. C. (2001). *Introduction to Modern Photogrammetry*,  
740 Hardcover (edition), New-York.
- 741 Monserrat, O., & Crosetto, M. (2008). Deformation measurement using terrestrial laser scanning  
742 data and least squares 3D surface matching. *ISPRS Journal of Photogrammetry and Remote*  
743 *Sensing*, 63, 142-154.
- 744 Moore J.F.A. (1992). Monitoring Building Structures. Blackie & Son Ltd. 155 p. ISBN 0-216-  
745 93141-X.
- 746 Oppikofer T., Jaboyedoff M., & Kreuzen H-R. (2008). Collapse at the eastern Eiger flank in the  
747 Swiss Alps. *Nature Geoscience*, 8, 531-535.
- 748 Pesci A., Baldi B., Bedin A., Casula G., Cenni N., Fabris M., Loddo F., Mora P., & Bacchetti M.  
749 (2004). Digital elevation models for landslide evolution monitoring: application on two areas  
750 located in the Reno River Valley (Italy). *Annals of Geophysics*, 47, 1339-1353.
- 751 Prokop, A., & Panholzer, H. (2009). Assessing the capability of terrestrial laser scanning for  
752 monitoring slow moving landslides. *Natural Hazards and Earth System Sciences*, 9, 1921-  
753 1928.

- 1
- 2
- 3 754 Rohaly J., Frigerio F., & Hart D. P. (2002). Reverse hierarchical PIV processing. *Measurement*
- 4 755 *Science and Technology*, 13, 984-996.
- 5
- 6 756 Squarzoni C., Delacourt C., & Allemand P. (2005). Differential single-frequency GPS monitoring
- 7 757 of the La Valette landslide (French Alps). *Engineering Geology*, 79, 215-229.
- 8
- 9 758 Sturzenegger, M., & Stead, D. (2009). Close-range terrestrial digital photogrammetry and
- 10 759 terrestrial laser scanning for discontinuity characterization on rock cuts. *Engineering*
- 11 760 *Geology*, 106, 163-182.
- 12
- 13
- 14 761 Tarchi, D., Casagli, N., Fanti, R., Leva, DD., Luzi, G., Pasuto, A., Pieraccini, M., & Silvano, S.
- 15 762 (2003). Landslide monitoring by using ground-based SAR interferometry: an example of
- 16 763 application to the Tessina landslide in Italy. *Engineering Geology*, 68, 15-30.
- 17
- 18
- 19 764 Teza, G., Galgaro, A., Zaltron, N., & Genevois, R. (2007). Terrestrial laser scanner to detect
- 20 765 landslide displacement fields: a new approach, *International Journal of Remote Sensing*, 28,
- 21 766 3425-3446.
- 22
- 23
- 24 767 Teza, G., Pesci, A., Genevois, R., & Galgaro, A. (2008). Characterization of landslide ground
- 25 768 surface kinematics from terrestrial laser scanning and strain field computation.
- 26 769 *Geomorphology*, 97, 424– 437.
- 27
- 28
- 29 770 Travelletti, J & Malet, J-P. Characterization of the 3D geometry of flow-like landslides: a
- 30 771 methodology based on the integration of multi-source data. *Submitted in Engineering*
- 31 772 *Geology*.
- 32
- 33
- 34 773 Wangensteen, B., Guomundsson, A., Eiken, T., Kääb, A., Farbrøt, H., & Etzelmüller, B. (2006).
- 35 774 Surface displacements and surface estimates for creeping slope landforms in Northern and
- 36 775 Eastern Iceland using digital photogrammetry. *Geomorphology*, 80, 59-79.
- 37
- 38
- 39 776 White, D. J., Take, W. A. & Bolton, M. D., (2003). Soil deformation measurement using particle
- 40 777 image velocimetry (PIV) and photogrammetry. *Géotechnique*, 53, 619-631.
- 41
- 42
- 43
- 44
- 45
- 46
- 47
- 48
- 49
- 50
- 51
- 52
- 53
- 54
- 55
- 56
- 57
- 58
- 59
- 60
- 61
- 62
- 63
- 64
- 65



1

2

3

4

5

6

7

8

9

10

11

12

13

14

15

16

17

18

19

20

21

22

23

24

25

26

27

28

29

30

31

32

33

34

35

36

37

38

39

40

41

42

43

44

45

46

47

48

49

50

51

52

53

54

55

56

57

58

59

60

61

62

63

64

65

1     **Correlation of multi-temporal ground-based images for**

2     **landslide monitoring: application, potential and limitations.**

3

4     Travelletti J. (1,2), Delacourt C. (3), Allemand P. (4), Malet J.-P. (1), Schmittbuhl J. (1),

5     Toussaint R. (1), Bastard M. (1)

6

7     (1) Institut de Physique du Globe de Strasbourg, CNRS UMR 7516, Université de Strasbourg /

8         EOST, 5 rue René Descartes, 67084 Strasbourg Cedex, France. E-mail:

9         julien.travelletti@unistra.fr

10    (2) GEOPHEN - LETG, CNRS UMR 6554, Université de Caen Basse-Normandie, Caen, France

11    (3) Institut Universitaire Européen de la Mer, CNRS UMR 6538, Université Européenne de

12         Bretagne, Brest, France.

13    (4) Laboratoire des Sciences de la Terre, CNRS UMR 5570, Université de Lyon & Ecole

14         Normale Supérieure, Lyon, France.

15

16     **Abstract**

17     The objective of this work is to present a low-cost methodology to monitor the displacement of

18     continuously active landslides from ground-based optical images analyzed with a normalized

19     Image Correlation technique. The performance of the method is evaluated on a series of images

20     acquired on the Super-Sauze landslide (South French Alps) over the period 2008-2009. The

21     image monitoring system consists in a high resolution optical camera installed on a concrete pillar

22     located on a stable crest in front of the landslide and controlled by a datalogger. The data are

23     processed with a cross-correlation algorithm applied on the full resolution images in the

24     acquisition geometry. Then, the calculated 2D displacement field is orthorectified with a back

25     projection technique using a high resolution DEM interpolated from Airborne Laser Scanning

26     (ALS) data. The heterogeneous displacement field of the landslide is thus characterized in time

27     and space. The performance of the technique is assessed using differential GPS surveys as

28     reference. The sources of error affecting the results are then discussed. The strongest limitations

29     for the application of the technique are related to the meteorological, illumination and ground

30     surface conditions inducing partial or complete loss of coherence among the images. Small

31     movements of the camera and the use of a mono-temporal DEM are the most important factors

32     affecting the accuracy of the ortho-rectification of the displacement field. Because the proposed

methodology can be routinely and automatically applied, it offers promising perspectives for operational applications like, for instance, in early warning systems.

**Keywords:** image cross-correlation; image matching; landslide; time-lapse photography; displacement monitoring

## 1 Introduction

Displacement monitoring of unstable slopes is a crucial tool for the prevention of hazards. It is often the only solution for the survey and the early-warning of large landslides that cannot be stabilized or that may accelerate suddenly. The choice of an adequate monitoring system depends on the landslide type and size, the range of observed velocity, the required frequency of acquisition, the desired accuracy and the financial constraints. Displacement monitoring techniques applied on landslides can be broadly subdivided in two main groups: geodetic and remote-sensing techniques.

Geodetic surveying consist in detecting geometrical changes in the landslide topography by measuring geometric parameters such as angles, distances or differences in elevation (e.g. levelling, tacheometry; Meissl & Naterop, 1995). These techniques necessitate the installation of targets in and outside the landslide and in measuring their position at different times. They have the advantage to be very accurate (0.2 to 2.0 cm) with a high potential of automation (Malet et al., 2002; Jaboyedoff et al., 2004; Foppe et al., 2006). Furthermore, many authors demonstrated the efficiency of permanent (Malet et al., 2002) and non-permanent (Squarzoni et al., 2005; Brunner et al., 2007) differential Global Positioning System (dGPS) for landslide monitoring with a centimetric accuracy during any daytime and weather conditions. However, because landslides can show highly variable displacement rates in time and space according to the local slope conditions (bedrock geometry, distribution of pore water pressures), the major drawbacks of the geodetic techniques are (1) to provide only discrete point measurements of the displacement and (2) the costs of installation and maintenance of the survey network. They are usually only justified in the case of a real risk for the population.

Remote-sensing techniques are interesting tools to obtain spatially-distributed information on the kinematics (Delacourt et al., 2007) and can be operational from spaceborne, airborne and ground-based platforms. Remote-sensing techniques give the possibility to discriminate stable and unstable areas and to map sectors within the landslide with different kinematics from a regional to a local scale. They are also useful tools for a process-based analysis of the deformation field affecting the slope (Casson et al., 2005; Teza et al., 2008; Oppikofer et al., 2008). In the last

decades, the development of ground-based platforms for landslide monitoring at the local scale provided many advantages over spaceborne and airborne platforms despite a shorter spatial coverage (Corsini et al., 2006). The geometry and frequency of acquisitions are more flexible and adaptable to any type of local environment. In addition permanent installations of ground-based platforms allow continuous monitoring (Casagli et al., 2004; Delacourt et al., 2007). Three main categories of ground-based remote sensing techniques are used in landslide monitoring: Ground-Based Synthetic Aperture Radar Interferometry (GB-InSAR), Terrestrial Laser Scanning (TLS) and Terrestrial Optical Photogrammetry (TOP). A non exhaustive review of the main advantages and disadvantages of these techniques is presented in Table 1. Detailed reviews of the application of GB-InSAR and TLS to landslides can be found in Luzi (2010), Corsini et al. (2006), Tarchi et al. (2003), Jaboyedoff et al. (2010), Teza et al. (2007, 2008) and Monserrat & Crosetto (2008). A state-of-the art of the application of TOP to landslide and related geomorphological processes is given below.

TOP is a technique with implementation, operating and equipment costs much lower than GB-InSAR and TLS. The technique consists in acquiring digital RGB images represented using a matrix of intensity values (brightness) recorded at each pixel of the Charge Coupled Device (CCD) of the camera from a spot very close to the ground (Jiang et al., 2008). In the last decades, camera self-calibration and analytical processing techniques allow the use of non-metric cameras and of simplified camera calibration algorithms to compute digital elevation models using the principle of stereoscopic views (Mikhail et al., 2001; Jiang et al., 2008). In the current state, the application of terrestrial images for landslide monitoring is mostly related to the production of DEMs for image ortho-rectification and sediment budget analysis (Bitelli et al., 2004, Pesci et al., 2004; Cardenal et al., 2008), and more recently to the characterization of the slope morpho-structure (Lim et al., 2005; Sturzenegger & Stead, 2009).

Using matching techniques, two-dimensional displacement fields can be derived by tracking objects in two images acquired at different time. So far, Image Correlation techniques have been applied only on aerial and satellite images (e.g. SPOT, QuickBird, OrbView, EROS) for the creation of landslide displacement maps (Casson et al., 2003; Delacourt et al., 2004; LePrince et al., 2008; Debella-Gilo & Käab, 2010). The use of Image Correlation on terrestrial images has not been as popular for permanent landslide monitoring as in other application field such as in solid and fluid mechanics for the characterization of the deformation pattern of soil/rock samples (White et al., 2003; Chambon et al., 2003; Küntz et al., 2005) or for the monitoring of other natural processes such as ice glaciers (Corripio et al., 2004; Fallourd et al., 2010; Maas et al., 2008) or volcanoes (Honda & Nagai, 2002). Only Delacourt et al. (2007) demonstrated an

efficient application of TOP for landslide monitoring which consisted in the determination of the landslide boundaries and in the qualitative estimation of the spatial variability of displacement at the La Clapière landslide (French Alps) with an image acquisition system installed at 1 km-distance.

Generally, the 2D displacements (in pixel) evaluated by the correlation algorithm have an accuracy of about 0.2 pixel (Casson et al., 2005; Delacourt et al., 2007) in the image plane, corresponding to an accuracy of millimeters to several centimeters for distances of about 100 m in the local coordinate system (Kraus & Waldhäusl, 1994).

The objective of this work is therefore to evaluate the potential and the limitations of TOP for the permanent monitoring of landslide using Image Correlation techniques. The dataset of images available for the Super-Sauze landslide (South French Alps) for the period 2008-2009 is used. First, the steps in the data acquisition and data processing (Image Correlation, ortho-rectification) are presented and the results are evaluated using the displacement of benchmark measured by dGPS. Second, the main advantages and disadvantages of the method and the influence of external factors on the precision and the accuracy of the results are discussed.

Throughout this work, the accuracy is defined as the systematic difference between a measured quantity and the true value, and precision is defined as the random difference between multiple measurements of the same quantity.

## 2 Experimental Site: the Super-Sauze landslide

To evaluate the potential of correlation of ground-based images for landslide monitoring, the dataset available at the Super-Sauze landslide, triggered in the Callovo-Oxfordian black marls of the South French Alps (Alpes-de-Haute-Provence, France; Fig. 1) is used. The landslide is located in the upper part of the Sauze torrential catchment. In the 1960s, the area was affected by rock failures in the scarp area. The failed material composed of rocky panels progressively transformed into a silty-sandy matrix integrating marly fragments of heterogeneous sizes through successive weathering cycles (Malet et al., 2003). From the 1970s until today, the landslide material is gradually filling a torrential stream with a typical range of displacement rate comprised between 1 to 3 cm.d<sup>-1</sup> on average and possible acceleration of up to 40 cm.d<sup>-1</sup> (Malet et al., 2002). In 2007, the mudslide extents over a distance of 920 m between an elevation of 1980 m at the scarp and 1760 m at the toe with an average width of 135 m and a average slope of 25°. The total volume is estimated at 560,000 m<sup>3</sup> (Travelletti & Malet, 2011-in press).

The kinematics of the landslide is currently monitored by differential Global Positioning System (dGPS), Terrestrial Laser Scanning (TLS) and by a remote camera monitoring system. This

instrumentation consists in a low-cost D70 Nikon reflex digital camera installed on a concrete pillar located on a stable crest in front of the landslide at a distance of 300 m from the lower part and 900 m from the main scarp (Fig. 1A, B, C). The acquisition system is controlled by a datalogger (Campbell CR10) and the power is provided by a 40 W solar panel. The characteristics of the acquisition are presented in Table 2. Every four days, a serie of images is acquired at 11:00, 12:00, 13:00 and 14:00 GMT in order to increase the probability of acquiring at least one image with good meteorological and illumination conditions. Each photograph (6 Mb) is stored in the Nikon native file format (NEF – Nikon Electronic Format) to avoid any loss of information.

### 3 Methodology

The steps in the data processing workflow consist in (1) correlating the images by pairs in their original acquisition geometry, and (2) orthorectifying the calculated displacement fields using a high-resolution digital elevation model interpolated from airborne LiDAR data. The images presenting the best ground texture contrast and the most homogeneous lightening are manually selected. The detailed methodology is summarized in Fig. 2 and described below.

#### 3.1 Principle of the Image Correlation technique

The 2D displacement field is obtained by correlating two optical images acquired at different time. The Image Correlation technique is based on the automatic identification of identical texture patterns within an image by maximizing a correlation function (Lewis, 1995; Baratoux et al., 2001; Debella-Gilo & Kääb, 2010). Its principle adapted for landslide kinematics analysis is described in Delacourt et al. (2007). Visible ground features have to be superimposed on two successive images on stable parts located outside the landslide. On the areas affected by landslide movements, the visible and recognizable features are shifted by the displacements. In order to quantify the ground displacements, a correlation window is defined on a reference (often the oldest) image. The corresponding window is searched in a pre-defined explored area belonging to the second image. The starting point of this explored area is the expected position of the window with the assumption that no displacement occurred between two acquisitions. The process is repeated for each pixel of the reference image. The Euclidean distance between the reference point and the matching point represents the displacement amplitudes in the image plane. By modifying the zone of interest, it is then possible to determine the displacements at various positions within the images. It is important to note that the normalized cross-correlation technique cannot track objects that start to rotate significantly or are affected by important perspective distortions (Lewis, 1995).

The size of the correlation window is a compromise between the desired accuracy on the displacement estimates and the spatial resolution of the velocity field (Delacourt et al., 2007). An increase of the size of the correlation window ensures a good signal to noise ratio and thus a good precision, but the accuracy on the displacement estimates decreases because of their averaging on a larger correlation window. This compromise is difficult to define when some parts of the landslide are well represented in terms of ground texture while others parts are not. Hierarchical correlation techniques allow one to overcome this problem by automatically changing the physical size of the correlation window and of the explored area during the correlation computations. The physical size is defined as the effective landslide surface covered by the correlation window (Rohaly, 2002; Aloui & Ibn-Elhaj, 2009).

In this work, a sub-pixel hierarchical correlation technique is used (Hild, 2003; Chambon, 2003; Bastard, 2009). The RGB images are first converted in gray-scale images on which a 3x3 pixel Sobel convolution matrix is applied to highlight the ground surface texture. The gradient values are then correlated (Chambon, 2003). Four successive degradations of the image resolution are applied following a pyramidal approach for changing the physical size of the correlation window and of the explored area by down-sampling the gradient values of the full resolution image (D'Antone, 1995; Kumar & Banerjee, 1998) (Fig. 3). The optimum sizes of the correlation window (16x16 pixels) and of the explored area (32x32 pixels) were identified with a trial and error procedure. These parameters are constant during the correlation computation. The correlation starts with the lowest resolution image in order to determine the largest displacements. Then the location of the pixel with the maximum cross-correlation value is used as the centre of the zone of interest for the next correlation step at a higher resolution. The spatial location of the maximum correlation value in the highest resolution image is thus progressively better estimated (Fig. 3). Ignoring high resolution information at the first computational step decreases the probability to reach a local minimum of the correlation function and, consequently, to obtain a wrong matching in the correspondence solution (Aloui & Ibn-Elhaj, 2009). In addition, this approach ensures very often a higher probability of detecting a reliable correlation peak (Anandan et al., 1993). The sub-pixel displacement is computed after the correlation at the highest resolution image. An iterative procedure is used to find the maxima of the correlation function interpolated with a bi-parabolic formula and with a maximization procedure based on the simplex method (Press et al., 1997; Chambon, 2003).

The correlation results consist in matrices of displacement  $\Delta u$  and  $\Delta v$  along the  $u$ - and  $v$ -axes in the image plane with their associated correlation index (Fig. 3). Because the pixel size is not constant in the image due to the oblique acquisition, the displacements field correlated in the

image plane cannot be directly interpreted in terms of metric displacements. Therefore an orthorectification procedure is necessary for a quantitative analysis of the displacement fields.

### **3.2 Ortho-rectification of the displacement field using high-resolution digital elevation models (DEMs)**

The orthorectification procedure consists in transforming the central projection of the image into an orthogonal view of the ground by correcting the effects of various distortion sources such as camera orientation, topographic effects and lens characteristics (Kraus & Waldhäusel, 1998). In terrestrial photogrammetry, distortions induced by topography effects are the most important due to the oblique acquisition of the images. The orthorectification converts the initial  $(u,v)$  and the final  $(u+\Delta u, v+\Delta v)$  positions of the displacement vectors in a local coordinate system. The conversion is possible if a Digital Elevation Model (DEM) of the object is available in order to relate two-dimensional pixel positions in the image plane to three-dimensional points in a local coordinate system using parametric approaches (Hemmle & Wiedemann, 1997).

In our approach, the rotation angles defining the external orientation of the camera are first determined using the relationship between the image coordinates  $(u,v)$  and the local coordinates system  $(X,Y,Z)$  given by the collinearity equations (Bonneval 1972, Kraus & Waldhäusel, 1994). These equations are based on the principle that each point in the local coordinate system is projected with a straight line through the projection center (origin of the camera) into the image plane. Knowing the exact location of the camera and assuming that the principal point coordinates is at the center of the image, the external angle and the effective focal length defining respectively the absolute orientation and the internal parameter of the camera can be determined with Ground Control Points (GCPs; Heikkilä & Silven, 1997; Corripio, 2004).

In our case, a serie of 95 pairs of GCPs distributed on the image plane and in the local reference system were measured with dGPS (Fig. 4). The centers of the GCPs are positioned in the local coordinate system with an average 3D accuracy of 0.02 m and a standard deviation of 0.01 m. The coordinates  $(u,v)$  of the GCPs in the image plane are determined by manual picking with an estimated accuracy of about 2 pixels. Among the 95 GCPs, 45 are used to compute the external parameters and 40 are kept to calculate the accuracy of the transformation (section § 5.2.1). A least mean square minimization technique based on a Direct Linear Transformation (DLT) and Singular Value Decomposition (SVD) between observed and calculated GCPs in the image plane is used to determine the external and internal parameters that satisfy the collinearity equations (Abdel-Aziz & Karara, 1971, Heikkilä & Silven, 1997).

Then, two DEMs (0.25m mesh-size, 3D error of 0.07 m) interpolated from Airborne Laser Scanning (ALS) dense point clouds acquired in October 2007 and July 2009 are used to orthorectify the displacements. A back projection of the DEMs is applied in the image plane using the external and internal parameters of the camera previously determined with the GCPs (Mikhail et al., 2001; Corripio, 2004). Only the points of the DEMs visible from the camera viewpoint are back projected to avoid duplicate points in the same position in the image plane. The sightline method is used to identify the visible points (Fig. 1C; Fisher, 1994; Franklin & Ray, 1994). About 57 % of the landslide area is visible from the camera view point. No displacements can be determined in the invisible areas. The 3D coordinates of the projected DEMs are then linearly interpolated in the image plane to allocate a triplet of  $X,Y,Z$  coordinates to each initial point  $(u,v)$  and each final point  $(u+\Delta u, v+\Delta v)$  of the correlated displacements. a re-projection of the displacement vector components in the local reference system is then applied. The displacement components in the local coordinate system are finally averaged and smoothed in a regular grid with a mesh size of 1m.

The use of a mono-temporal DEM for the orthorectification of the initial point  $(u,v)$  and the final point  $(u+\Delta u, v+\Delta v)$  of the displacement vectors is a strong hypothesis that the global landslide morphology remains constant over the period. It affects the accuracy of the transformation of the displacement vector in the local coordinate system. However, it will be further demonstrated that this method is still a relevant estimation for our purpose with reference to the amplitude of the observed displacements (section § 4.2).

### 3.3 Image resolution at the terrain surface

The effective (e.g. ground) pixel size is one of the limiting parameters for the accuracy of the correlation (Fig. 5A). It determines the minimum theoretical displacement that can be detected for a pixel-level correlation. Below this displacement threshold, the accuracy solely depends on the accuracy of the sub-pixel correlation. The effective pixel size depends on (1) the distance between the object and the camera and (2) the angle of incidence which is defined as the complementary angle between the line of sight of the camera and the normal to the terrain surface (Fig. 5B). A low incidence angle means that the line of sight is nearly tangential to the topography.

Globally, the incidence angle on the landslide ranges from  $0^\circ$  to  $40^\circ$  and the pixel size varies from  $1.10^{-2} \text{ m}^2$  in the lower part (at an average distance of 300m) to  $3.10^{-2} \text{ m}^2$  in the upper part of the landslide (at an average distance of 900 m; Fig. 5A,B). The upper part is characterized with a pixel size often larger than  $0.04 \text{ m}^2$ , especially in areas where the angle of incidence is less than  $5^\circ$ . Therefore the lowest accuracy is expected in this region because the detection of small  $\Delta v$  and



$\Delta u$  displacements can correspond to important  $\Delta X$ ,  $\Delta Y$ ,  $\Delta Z$  metric displacement. Approximately half of the number of pixels in the image plane inside the landslide area show a metric sensitivity of less than 0.17 m for one pixel displacement along the  $v$ -axis and of less than 0.07 m along the  $u$ -axis. The minimum displacements for a pixel-level correlation in respectively the  $u$  and  $v$ -direction are 0.04 m and 0.06 m in the lower part of the landslide and 0.09 m and 0.11 m in the upper part. In areas where the incidence angle is less than  $5^\circ$ , the minimum displacement that can be detected drastically increases. Therefore no strong confidence is given to areas whose incidence angle is lower than  $5^\circ$ .

### 3.4 Post-processing: displacements filtering

Filtering criteria are necessary to remove the badly correlated points and improve the signal to noise ratio (Casson et al., 2003; Berthier et al., 2005; Wangenstein et al., 2006; Debella-Gilo & Kääb, 2010). Three criteria are used in this work to filter aberrant displacements in the image plane coordinate system and in the local coordinate system. There are based on:

1. the value of the correlation peak coefficient: loss of coherence can occur during the computations because changes in surface states between a reference image and the correlated image are high, resulting thus in low correlation coefficients. Defining a threshold value has the consequence to increase the percentage of realistic displacements. A high threshold coefficient of  $r=0.6$  was selected to remove the badly correlated points. However, the correlation peak coefficient alone is not a sufficient discriminating criterion because some points can display a high correlation coefficient even if they do not represent the same object (e.g. two trees or large stones having the same geometry; Casson et al., 2005);
2. the value of displacement amplitude and direction: points characterized by upslope displacement and important displacement amplitude with reference to a priori knowledge on the landslide kinematics are filtered.
3. the displacements assigned to invisible points from the camera viewpoint because of small orthorectification errors in the conversion to the local coordinate system.

Table 3 presents the results of the filtering on the total number of correlated points. Displacements correlated from images acquired in the summer season (23–27 July 2008) and in the autumn season (19–23 October 2008) highlight the differences in the number of remaining values for the two seasons. The amount of remaining point after filtering varies between 80% and 90% in the summer period and can decrease to 50% in the autumn period. This is mainly explained by the different illumination conditions (low sun elevation) that affect the quality of the

correlation. This aspect will be discussed further in section §6.1.3. The upper part of the landslide is the most affected by the filtering. This area generally shows a percentage of remaining values lower than in the middle and lower parts of the landslide. This is explained by the fact that the upper part has a more chaotic morphology. Consequently the effects of illumination changes are more important than in the middle and the lower parts, especially in autumn. In addition, the angle of incidence in this area can be low (5 to 10°) and thus sensitive to slight movements of the camera.

## 4 Results

### 4.1 Displacement maps of the landslide

A set of images over the period May–July 2008 is used to illustrate the potential of the technique for the characterization of the kinematics during an acceleration period triggered by high rainfall amounts and a fast melting of the snow cover.

Figure 6 shows an example of displacement rate (in  $\text{pixel.day}^{-1}$ ) of the ground surface in the image plane derived from image pairs of 20–28 May, 1–4 June and 9 June–13 June. The reference is the image of 20 May. The contrast in displacement rates between the landslide area and the stable area gives confidence on the calculated velocity field. One can notice that the pattern of displacement rate is heterogeneous spatially and temporally. The upper part of the landslide displays the highest velocity ranging from 1 to 7  $\text{pixels.day}^{-1}$  while the lower part displays velocity of less than 4  $\text{pixels.day}^{-1}$ . No quantitative comparisons can be carried out at this stage because the pixel sizes vary strongly in the image (Fig. 5A). From the 20 May to the 13 June, cumulated displacements up to 110 pixels are observed in the upper part. The maximum of displacement rate is observed around the 1<sup>st</sup> June. Then the landslide decelerates to displacement rate of about 1  $\text{pixel.day}^{-1}$ .

Some local specific displacement patterns are also clearly highlighted. For instance, the presence of a stable *in-situ* crest located in the landslide body is perfectly identified in the correlated images.

Figure 7 presents the amplitude of the 3D orthorectified displacement rates for the period 1–4 June in the local coordinate system. The difference of kinematics between the upper (until 3  $\text{m.day}^{-1}$ ) and the lower (until 1  $\text{m.day}^{-1}$ ) parts becomes more evident than in the image plane. The geometrical effect induced by the presence of the stable *in-situ* crest on the landslide kinematics is also clearly pointed out. The temporal evolution of the displacement rates is illustrated with two transversal profiles and one longitudinal profile on Figures 7 and 8. The

difference of displacement rates between the upper and the lower part of the landslide is particularly pointed out.

The precision of the computed displacements is assessed by performing a null hypothesis on the stable areas (Berthier et al., 2005; Casson et al., 2003). Only the points with a correlation coefficient  $r > 0.8$  are taken into account. In the image plane coordinate system, the average error  $\mu$  range from 0.5 to 0.9 pixels with standard deviation  $\sigma$  of 0.3 to 1.2 pixels for the image pairs between the 20 May and the 25 June. In the local coordinate system, the average error  $\mu$  range from 0.03 m to 0.11 m with standard deviation  $\sigma$  of 0.10 to 0.31 m for the image pairs between the 20 May and the 25 June.

## 4.2 Comparison with dGPS displacements

Sixty benchmarks distributed in the stable parts and on the landslide body were monitored by dGPS (horizontal and a vertical average accuracy of  $\pm 0.02$  m and  $\pm 0.05$  m) to estimate the accuracy and validate the displacements obtained from the Image Correlation. In total, 219 DGPS measurements are available for the period 2008–2009. In order to validate the displacements computed in the image plane, the dGPS benchmarks are projected in the image plane using the collinearity equations. The pixel displacements derived from the Image Correlation are then averaged in a perimeter of 16 pixels around each benchmark. The results are presented in Figure 9A. A correlation coefficient of  $r = 0.98$  is found between dGPS measurements and Image Correlation, and an average relative accuracy of 11% is determined (Fig. 9C). In order to validate the metric displacements in the local coordinate system, the orthorectified displacements are averaged in an area of  $4 \text{ m}^2$  around each benchmark and compared with the dGPS displacements. A correlation coefficient of  $r = 0.95$  is found (Fig. 9B), and an average relative accuracy of 20% is determined (Fig. 9D). The reason why the correlation coefficient in the orthorectified case is lower than in the pixel case is believed to be related to the accuracy of the DEM used for the orthorectification. This will be discussed in section §5.2.2.

## 5 Discussion: sources of errors

The major sources of errors affecting the displacement calculations and thus limiting the efficiency of TOP for an operational landslide monitoring can be classified in two groups: (i) the parameters affecting the Image Correlation computation and (ii) the external parameters influencing the orthorectification procedure.

## 5.1 Sources of errors affecting the Image Correlation computation

### 5.1.1 Accuracy and precision of the Image Correlation algorithm

One limitation of the Image Correlation technique is directly linked to the correlation algorithm and the sub-pixel interpolation method (Debella-Gilo & Käab, 2010). A series of experimental tests were carried out to assess the precision of the Image Correlation technique. The series of tests allow one to investigate the influence of the size of the correlation window and of the level of noise observed in the images. Homogeneous imposed displacements (systematically equal to a multiple of pixels to avoid image resampling; Chambon & Schmittbuhl, 2003) are applied to pairs of images to create synthetic images. Furthermore, three levels of Gaussian noise were added to the original images with a mean noise level imposed to zero and variances  $\sigma^2$  imposed to  $10^{-4}$ ,  $10^{-3}$  and  $10^{-2}$  (Fig. 10A). Then the Image Correlation technique is applied on the original image taken as reference and on the synthetic image with different sizes of correlation windows (5, 10, 16, 20, 30 and 50 pixels). For each correlation window, fifteen imposed displacements were calculated with amplitudes ranging from 1 to 23 pixels along the  $u$  and  $v$ -directions. The analysis was conducted by comparing the noisy synthetic images with the reference image. In the optimal case, the measured displacement would be identical to the imposed displacement.

Each Image Correlation analysis revealed displacement differences distributed close to zero (mean accuracy of  $5 \cdot 10^{-4}$  pixels). As observed by Hild et al. (2003), the precision of the correlation algorithm mainly depends on the pixel fraction of the displacement. Larger correlation windows produce less scattered displacements and therefore improve the precision. By plotting the standard deviation of the calculated displacements against the size of the correlation window, the influence of the correlation window size can be pointed out (Fig. 10B). For very low level of noise, the precision is less than 0.1 pixels for a size of correlation window greater than 5x5 pixels. For higher level of noise, the precision is more dependent on the size of the correlation window. Because homogenous displacements field were imposed in the image, the accuracy (average misfit) is similar for small and large correlation windows. In reality, the displacement field becomes more heterogeneous at higher resolution. Therefore, an increase of the size of the correlation window implies a decrease of the spatial resolution but, as shown in these tests, an increase of the precision.

### 5.1.2 Influence of ground surface state

The time lag between two image acquisitions is one of the critical factors that affect the correlation computation. This time has to be long enough to increase the signal (e.g. landslide

displacement) but short enough to preserve the tracked features (Berthier et al., 2005). Loading of the snowpack on the ground during winter, surface erosion due to fast snow melting and the development of water-saturated ponds in spring, weathering of the objects, growing of grass and large deformations are environmental processes that significantly modify the surface state during a year. Such correlation errors are characterized by very low correlation coefficients, very large displacement amplitudes or randomly-distributed displacement directions in comparison to the neighbor pixels (Fig. 11). On average, about 20 to 25% of the points are usable from one year to the next year (using a correlation window of 16\*16 pixels and with a correlation coefficient threshold of 0.8). Consequently, the construction of long time series of displacements with the Image Correlation technique is a difficult task for the site. The range of cumulated displacement rates observed over a period of 16 months (May 2008–September 2009) is illustrated by tracking the displacement at three locations in the upper (pt 1), middle (pt 2) and lower (pt 3) parts of the landslide at the direct vicinity of benchmark measured by dGPS (Fig. 7). In our case, the cumulated displacements of the year 2009 are adjusted on those of 2008 using GCPs measured with dGPS at the vicinity of the points pt1, pt2 and pt3. The monitoring of a few benchmark with geodetic techniques is therefore necessary to combine displacement pattern observed in image pairs acquired over the period May 2008–September 2009 (74 pairs of images). After the acceleration period of spring 2008, the displacement rates are decreasing to a relative constant values of about 0.02 m.day<sup>-1</sup> in the lower and middle parts and 0.05 m.day<sup>-1</sup> in the upper part computed over the period July to October (Fig 12).

### 5.1.3 Influence of illumination conditions

The difference observed in RGB intensities in various images acquired with various solar illumination angles is an important limiting factor essentially in terms of changes of the shadow areas (Berthier et al., 2005). In order to assess the influence of illumination conditions on the Image Correlation results, two experiments are carried out.

The first experiment consists in correlating images acquired at different times within a day. Four photographs acquired at 11:00, 12:00, 13:00 and 14:00 GMT in a period of low displacements (< 0.02 m.day<sup>-1</sup>, August 2009) and of clear sky conditions are correlated. The results indicate that illumination changes can lead to an average  $\mu$  and a standard deviation  $\sigma$  of pixel-level error of respectively  $\mu_{1h}=1.31$  and  $\sigma_{1h}=0.03$ ,  $\mu_{2h}=1.35$  and  $\sigma_2=0.12$ ,  $\mu_{3h}=1.89$  and  $\sigma_{3h}=0.18$  pixel for time-interval acquisition of respectively 1, 2 and 3 hours. The results demonstrate that the correlation of images acquired in nearly similar illumination conditions can display a pixel-level precision.

The second experiment consists in creating synthetic images with different shadow intensities as a function of the sun azimuth and elevation (Burrough & McDonell, 1988). Only the shadows created by direct solar illumination are analyzed assuming clear-sky conditions. The effects of reflected and diffuse illuminations are neglected. Ninety seven shaded relief images were created with different artificial illuminations (eg. Fig. 4). Because a preference is given to correlate images taken when the sun elevation is maximal (Delacourt et al., 2007), a shaded relief image with a sun elevation of  $65^{\circ}$  and a sun azimuth of  $250^{\circ}$  (illumination coming from the South-West in July at 12:00 GMT) is chosen as the reference image for the correlation. The reference image is correlated with the shaded relief images. The mean correlation coefficient is used to characterize the influence of illumination changes on the image.

As expected, the correlation of the synthetic images indicates that the correlation coefficient strongly depends on the sun elevation and the sun azimuth (Fig. 13). Illumination coming from the opposite direction of the one of the reference (sun azimuth of  $120^{\circ}$ ) with low elevation angles ( $<30^{\circ}$ : end of the daytime in autumn) provide the less reliable correlation results. This finding is in agreement with Table 2 which indicates that the amount of interpretable displacements is lower in the autumn season than in the summer season (lower correlation coefficients). Therefore, correlation of images with a too important time-lapse has to be avoided to minimize illumination effects. A possible alternative is to correlate images under diffused illumination (cloudy day) thus providing a more homogenous lightning. At the opposite, correlation of images acquired at the same solar time in the day and when the sun elevation is maximal is optimal.

In order to compensate for the loss of reliable results in certain areas of the landslide due to strong illumination and ground surface changes, displacements can be interpolated from more reliable neighbor results according to a weight depending on the correlation coefficient (Niebling et al., 2010).

## **5.2 Sources of errors affecting the ortho-rectification procedure**

### **5.2.1 Influence of camera orientation**

The accuracy of the camera orientation is a parameter affecting both the image geometry and the accuracy of the orthorectification (Mikhail et al., 2001). If changes in external orientation of the camera are small, the image geometry is not significantly affected. Consequently a homogeneous component in the correlated displacement field is visible in the image plane (Fig. 14A). This misfit can be significant in the areas where the expected displacements are low or null such as in the stable parts. This systematic error can be corrected assuming a rigid translation of the image

by removing the average  $\Delta u$  and  $\Delta v$  misfits (observed on the stable parts of the images such as stable crests or on reference targets located outside the landslide; Fig. 1B, A; Fallour et al., 2010). Nevertheless this correction is not fully optimal, because the geometric deformations caused by the slight movements of the camera depend on the object distance. Therefore, after correction of the homogeneous component in the image plane, an average residual misfit of about 0 to 2 pixels is observed.

In order to evaluate the accuracy of the external orientation that influences the orthorectification quality, forty GCPs not introduced in the minimization processes of section §3.2.3 are used. The shift between the projected and the observed GCPs positions in the image plane is thus determined (Fig. 14B). A mean shift error of, respectively, -0.20 and -0.08 pixel with a standard deviation of 1.59 and 1.51 pixels in the  $u$  and  $v$ -directions is obtained (Table 4). The accuracy of the external parameters in the orthorectification procedure in the local coordinate system is calculated by comparing the back-projected GCPs identified in the image plane with the GCPs positions measured with DGPS and located in the stable parts. The absolute accuracy in  $X$ ,  $Y$  and  $Z$  coordinates are presented in Table 4. Because most of GCPs in the stable parts are located in the background of the image where the ground pixel size is about 0.20 m, the mean 3D error (0.14 m) and the standard deviation (0.56 m) of the positioning are not representative of the areas of the landslide located closer to the camera (300 m). Nevertheless, because the standard deviation of the GCPs located in the image plane are close to the accuracy of the GCPs picking, the determination of the camera orientation is considered acceptable. Furthermore, the good coherence between the shaded relief images (Fig. 4) and the true images (Fig. 1B) shows that the quality of the determination of the camera orientation is satisfying.

### 5.2.2 Influence of the DEM

In order to evaluate the influence of the DEM on the orthorectified displacements, the displacements of the period 1–4 June 2008 originally orthorectified with the DEM of October 2007 (Fig. 7) are compared with those orthorectified with the DEM of July 2009 (Fig. 15A, B). The observed differences in displacement are presented relative to the displacement orthorectified with the DEM of 2007. The differences vary spatially in the landslide area. Despite some areas displaying differences in displacement larger than 75%, the average difference is 21% which is very similar to the differences observed with the dGPS measurements (Fig. 9D). As a consequence, the influence of the DEM on the accuracy of the displacement is more important than the influence of the camera orientation, the image resolution and changes in illumination conditions. For large displacements, morphologic changes become significant and the errors on

the displacements increase. The computation of multi-temporal DEMs for each image is therefore a pre-requisite to improve the accuracy of the orthorectified displacements. Nevertheless, in case of a translational landslide characterized by low changes in elevation, the use of the same DEM constitutes still an acceptable 1<sup>st</sup>-order estimate.

## 6 Conclusion

The potential of multi-temporal correlation of ground-based images for landslide monitoring has been assessed using the dataset available on the Super-Sauze landslide (South French Alps). A methodology to compute displacement rates both in the image plane coordinate system and in the local coordinate system is proposed.

The results demonstrated clearly the potential and the limitation of this technique by identifying the heterogeneous displacement field of the landslide in space and in time. The camera monitoring allowed one to characterize displacements of up to 3 m.day<sup>-1</sup> during an acceleration period, and displacement of about 0.02 m.day<sup>-1</sup> over the decelerating period of July to September. The results are in good agreement with previous knowledge on the landslide kinematics and are in very good agreement with benchmark displacements measured by dGPS.

For objects located in a range of 300 to 900 m from the camera location, this study showed that the pixel size can vary from 0.005 to 0.04 m<sup>2</sup> according to the resolution of the image (2000x3008 pixels) and the angle of incidence of the line of sight. The orientation of the line of sight to the ground surface has to be considered before installing a permanent monitoring system. Areas of low incidence angles (<5°) are very sensitive to small movements of the camera. Therefore, the angle should be the most perpendicular as possible to the mean displacement vector of the landslide. 3D displacements of less than 0.04 m and 0.06 m in the lower part of the landslide and 0.09 m and 0.11 m in the *u* and *v*-directions over a period of four days are impossible to detect without the use of sub-pixel correlation algorithms. However, the sources of errors due to small movement of the camera and the use of a mono-temporal DEM are the main limiting factors. A regular acquisition of multi-temporal DEMs through airborne or terrestrial laser scanning or stereoscopic photogrammetric views is believed to be a priority to significantly improve the accuracy of the technique. The errors induced by the sub-pixel correlation algorithm are thus insignificant compared to the influences of the other parameters cited previously.

The strongest limitations are independent of the acquisition system. They are related to the meteorological and illumination conditions and the ground surface changes inducing partial or complete loss of coherence between image pairs. During the winter season (from November to May), the presence of snow impedes reliable correlation results while excessive ground



displacements between two consecutive years impede valid displacement measurements even if the images are acquired during the same solar time.

The results demonstrate that Image Correlation techniques implemented in permanent monitoring system are particularly interesting for monitoring landslides characterized by annual pluridecimetric displacements. In addition, this low-cost technique is a very suitable alternative for inaccessible landslides or areas without access to power supply. Furthermore, because the proposed methodology does not require GCPs except for the calibration of the camera and for combining displacement pattern observed in image pairs acquired over two years, the methodology can be routinely and automatically applied to new image pairs. Therefore this work offers very promising perspectives for operational applications which can be potentially integrated in early warning systems by considering additional efforts in direct data transmission. Finally, inversion of the displacement field could be developed to characterize the macroscopic rheological properties of the landslide material.

## Acknowledgements

This work was supported by the European Commission within the Marie Curie Research and Training Network ‘*Mountain Risks: from prediction to management and governance*’ (2007-2010, Contract MCRTN-035798) and by the FP7 Large-scale Integrating Project ‘*Safeland: Living with landslide risk in Europe*’ (2009-2012, Contract 226479). The ortho-images and the airborne LiDAR data of the Super-Sauze landslide have been acquired by the Sintegra company in 2007 and by the Helimap System service in 2009. The authors would like to acknowledge André Stumpf (University of Strasbourg, France & University of Twente, Netherlands) and Sabrina Rothmund (University of Stuttgart, Germany) for their help in the field. Special thanks are also due to Bas van Dam (Utrecht University, Netherlands) who designed the automatic monitoring system. The authors are also grateful to Prof. C. Gökçeoğlu and an anonymous reviewer for their constructive comments.

## References

- Abdel-Aziz, Y. I. & Karara, H. M. (1971). Direct linear transformation into object space coordinates in close-range photogrammetry. *Proc. Symposium on Close-Range Photogrammetry*, Urbana, Illinois, 1-18.

- Anandan, P., Bergen, R.J., Hanna, K.J., & Hanna, K.J. (1993). Hierarchical model-based motion estimation. In L. Sezan, (Eds.), *Image Sequence Analysis*. Kluwer, Dordrecht.
- Antonello, G., Casagli, N., Farina, P., Leva, D., Nico, G., Sieber, A.J., & Tarchi, D. (2004). Ground-based SAR interferometry for monitoring mass movements. *Landslides, 1*, 21-28.
- Baratoux, D., Delacourt, C., & Allemand, P. (2001). High-resolution digital elevation models derived from Viking Orbiter images: Method and comparison with Mars Orbiter Laser Altimeter Data. *Journal of Geophysical Research, 106*, 32927-32941.
- Bastard, M., (2009). Caractérisation de la cinématique de glissement de terrain par technique de corrélation d'image optique. Master thesis. University of Strasbourg (EOST). Institut de Physique du Globe, Strasbourg, France.
- Berthier, E., Vadon, H., Baratoux, D., Arnaud, Y., Vincent, C., Feigl, K. L., Rémy, F., & Legrésy, B. (2005). Surface motion of mountain glaciers derived from satellite optical imagery. *Remote Sensing of Environment, 95*, 14-28.
- Besl, P., & McKay, N. (1992). A method for registration of 3-D shapes. *IEEE Transactions on Pattern And Machine Intelligence, 14*, 239-256.
- Bitelli, G., Dubbini, M., & Zanutta, A. (2004). Terrestrial laser scanning and digital photogrammetry techniques to monitor landslides bodies, *International Archives of Photogrammetry, Remote Sensing and Spatial Information Sciences 35*, 246–251.
- Bonneval, H., (1972). Levés topographiques par photogrammétrie aérienne. In Eyrolles (Eds.), *Photogrammétrie générale: Tome 3, Collection scientifique de l'Institut Géographique National*, Paris, France.
- Brunner, F., Macheiner, K., & Woschitz, H. (2007). Monitoring of deep-seated mass movements. *Proceedings of the 3rd International Conference on Structural Health Monitoring of Intelligent Infra-structure*, Vancouver, Canada.
- Burrough, P. A., & McDonell, R.A. (1998). *Principles of Geographical Information Systems*, Oxford University Press, New York.
- Cardenal, J., Mata, E., Perez-Garcia, J.L., Delgado, J., Andez, M.A., Gonzalez, A., Diaz-de-Teran, J.R. (2008). Close Range Digital Photogrammetry Techniques applied to Landslide Monitoring. *International Archives of the Photogrammetry, Remote sensing and Spatial Information Sciences*. Vol XXXVII. Part B8.
- Casagli, N., Farina, P., Leva, D., & Tarchi, D. (2004). Application of ground-based radar interferome-try to monitor an active rock slide and implications on the emergency management. In E. Kluwer (Eds.), *The NATO Advanced Research Workshop*, Celano, Italy.

- 586 Casson B., Delacourt C., & Allemand, P. (2005). Contribution of multi-temporal sensing images  
587 to characterize landslide slip surface – Application to the La Clapière Landslide (France).  
588 *Natural Hazards and Earth System Sciences*, 5, 425-437.
- 589 Casson, B., Baratoux, D., Delacourt, D., & Allemand, P. (2003). “La Clapière” landslide motion  
590 observed from aerial differential high resolution DEM. *Engineering. Geology*, 68, 123-139.
- 591 Chambon, G., & Schmittbuhl, J. (2003). Shear with comminution of a granular material:  
592 Microscopic deformations outside the shear band. *Physical Review E*, 68, 1-8.
- 593 Chambon, G. (2003). Caractérisation expérimentale du frottement effectif des zones de faille.  
594 PhD Thesis. Université Paris XI Orsay, ENPC..
- 595 Corripio, J.G. (2004). Snow surface albedo estimations using terrestrial photography.  
596 *International Journal of Remote Sensing*, 25(24), 5705-5729.
- 597 Corsini, A., Farina P., Antonello G., Barbieri M., Casagli N., Coren F., Guerri L., Ronchetti F.,  
598 Sterzai P., & Tarchi D. (2006). Space-borne and ground-based SAR interferometry as tools  
599 for landslide hazard management in civil protection. *International Journal of Remote*  
600 *Sensing*, 27, 2351 - 2369.
- 601 D’Antone, I. (1995). Hierarchical correlation for track finding. *Nuclear Instrument and Methods*  
602 *in Physics Research*, 356, 476-484.
- 603 Debella-Gilo M., & Kääb, A. (2010). Sub-pixel precision image matching for measuring surface  
604 displacements on mass movements using normalized cross-correlation. *Remote Sensing of*  
605 *Environment* (2010).
- 606 Delacourt, C., Allemand P., Casson B., & Vadon H. (2004). Velocity field of the “La Clapière”  
607 landslide measured by the correlation of aerial and Quick-Bird satellite images. *Geophysical.*  
608 *Research Letters*, 31, 1-5.
- 609 Delacourt, C., Allemand, P., Berthier, E., Raucoules, D., Casson, B., Grandjean, P., Pambrun, C.,  
610 & Varel, E. (2007). Remote-sensing techniques for analysing landslide kinematics: a review.  
611 *Bulletin de Société Géologique*, 178, 89-100.
- 612 El Alaoui El., M. I., & Ibn-Elhaj, E. (2009). A robust hierarchical motion estimation algorithm in  
613 noisy image sequences in the bispectrum domain. *Signal Image and Video Processing*, 3,  
614 291-302.
- 615 Fallourd, R., Vernier, F., Friedt J.-M., Martin, G., Trouvé, E., Moreau, L. & Nicolas, J.-M.  
616 (2010). Monitoring temperate glacier with high resolution automated digital cameras –  
617 Application to the Argentière Glacier. In: Paparoditis N., Pierrot-Deseilligny M., Mallet  
618 C. & Tournaire O. (Eds.), IAPRS, Vol. XXXVIII, Part 3B, Saint-Mandé, France., 1-23.

- 1
- 2
- 3
- 4 619 Fisher, P.F. (1991). First experiments in viewshed uncertainty: The accuracy of the viewshed
- 5
- 6 620 area. *Photogrammetric Engineering Remote Sensing*, 57, 1321-1327.
- 7
- 8 621 Foppe, K., Barth, W., & Preis, S. (2006). Autonomous Permanent Automatic Monitoring System
- 9 622 with Robot-Tacheometers. *Proceedings of the XXIII International FIG Congress*, Munich,
- 10 623 Germany.
- 11
- 12 624 Franklin, W.R., & C.K. Rav. (1994). Higher isn't necessarily better: Visibility algorithms and
- 13
- 14 625 experiments, *Proceedings of the 6<sup>th</sup> International Symposium on Spatial Data Handling*,
- 15 626 Edinburgh, Scotland, 2, 751-770.
- 16
- 17 627 Heikkila, J., & Silven, O. (1997). A four-step camera calibration procedure with implicit image
- 18 628 correction. *IEEE Computer Society*, 1106-1112.
- 19
- 20 629 Hemmleb, M., & Wiedemann, A. (1997). Digital Rectification and Generation of Orthoimages in
- 21 630 Architectural Photogrammetry. *CIPA International Symposium*, IAPRS, XXXII, Part 5C1B
- 22 631 (pp. 261-267), Göteborg, Sweden., 261-267.
- 23
- 24 632 Hild, F. (2003). Mesure de champs de déplacement par corrélation d'images et applications en
- 25 633 mécanique des solides. *Notes de cours IPSI*. Laboratoire de Mécanique et Technologie,
- 26 634 CNRS-UMR 8535, Université Paris 6, France.
- 27
- 28 635 Honda, K., & M. Nagai, M. (2002), Real-time volcano activity mapping using ground-based
- 29 636 digital imagery, *ISPRS Journal of Photogrammetry and Remote Sensing*, 57,1-2, 159-168.
- 30
- 31 637 Jaboyedoff, M., Oppikofer T., Abellan A., Derron M.-H., Loye A., Metzger R., & Pedrazzini A.
- 32 638 (2010). Use of LiDAR in landslide investigations : a review. *Natural Hazards*. doi
- 33 639 10.1007/s11069-010-9634-2
- 34
- 35 640 Jaboyedoff, M., Ornstein, P., & Rouiller, J.-D. (2004). Design of a geodetic database and
- 36 641 associated tools for monitoring rock-slope movements: the example of the top of Randa
- 37 642 rockfall scar. *Natural Hazards and Earth System Science*, 4, 187-196.
- 38
- 39 643 Jiang, R., Jauregui, D.V., & White, K. (2008). Close-range photogrammetry applications in
- 40 644 bridge measurement: Literature review. *Measurement*, 41, 823-834.
- 41
- 42 645 Kraus, K. & Waldhäusl, P., (1994). *Photogrammetry, Fundamentals and Standard processes*.
- 43 646 vVol . 1. Hermès (editor), Paris.
- 44
- 45 647 Kumar, S., & Banerjee, S., (1998). Development and application of a hierarchical system for
- 46 648 digital particle image velocimetry to free-surface turbulence. *Physics of Fluids*, 10, 160-177.
- 47
- 48 649 Küntz, M., Jolin, M., Bastien, J., Perez F., & Hild, F. (2007). Digital image correlation analysis of
- 49 650 cracks behavior in a reinforced concrete beam during a load test. *Canadian journal Journal of*
- 50 651 *civil Civil engineeringEngineering*, 33, 1418-1425.
- 51
- 52
- 53
- 54
- 55
- 56
- 57
- 58
- 59
- 60
- 61
- 62
- 63
- 64
- 65

- 652 LePrince, S., Berthier, E., Ayoub, F., Delacourt, C., & Avouac, J.- P. (2008). Monitoring Earth  
653 earth Surface surface Dynamics dynamics With with Optical Imagery. *Eos*, 89, 1-5.
- 654 Lewis, J.P., (1995). Fast normalized cross-correlation. *Vision Interface*, 120-123.
- 655 Lim, M., Petley, D.N., Rosser, N.J., Allison, R.J., Long, A.J. & Pybus, D. (2005). Combined  
656 digital photogrammetry and time-of-flight laser scanning for monitoring cliff evolution. *The*  
657 *Photogrammetric Record*, 20, 109-129.
- 658 Luzi, G., (2010). Ground based SAR interferometry: a novel tool for Geoscience. In: Geoscience  
659 and Remote Sensing, New Achievements, P.Imperatore & D. Riccio (EditorsEds.), ISBN:  
660 978-953-7619-97-8. In print.
- 661 Maas, H.-G., Schwalbe, E., Dietrich, R., Bässler, M., & Ewert, H. (2008). Determination of  
662 spatio-temporal velocity fields on glaciers in West- Greenland by terrestrial image sequence  
663 analysis. *IAPRS*, XXXVII, Part B8 Beijing,China, 1419-1424.
- 664 Malet, J.-P. (2003). Les glissements de type écoulement dans les marnes noires des Alpes du Sud.  
665 Morphologie, fonctionnement et modélisation hydromécanique. PhD Thesis in Earth  
666 Sciences, Université Louis Pasteur, Strasbourg.
- 667 Malet, J.-P., Maquaire, O., & Calais, E. (2002). The use of global positioning system techniques  
668 for the continuous monitoring of landslides. *Geomorphology*, 43, 33-54.
- 669 Mantovani, F., Soeters, R., & van Western, C.J. (1996). Remote sensing techniques for landslide  
670 studies and hazard zonation in Europe. *Geomorphology*, 15, 213-225.
- 671 Meissl, A., & Naterop, D. (1995). Automatic Measuring System for Permanent Monitoring –  
672 Solexperts GeoMonitor. *Proceedings of Field Measurements in Geomechanics 4th*  
673 *International Symposium*, Bergamo, Italy, 489-494.
- 674 Mikhail, E., Bethel, J. S., & McGlone, J. C. (2001). *Introduction to Modern Photogrammetry*,  
675 Hardcover (edition), New-York.
- 676 Monserrat, O., & Crosetto, M. (2008). Deformation measurement using terrestrial laser scanning  
677 data and least squares 3D surface matching. *ISPRS Journal of Photogrammetry and Remote*  
678 *Sensing*, 63, 142-154.
- 679 Moore, J.F.A. (1992). Monitoring bBuilding sStructures. Blackie & Son Ltd.. , 155 p. ISBN 0-  
680 216-93141-X.
- 681 Niebling, M.J., Flekkøy E.G., Måløy K.J., & Toussaint, R. (2010). Mixing of a granular layer  
682 falling through a fluid. *Physical Review E* , 82, 011301. doi: 10.1103/PhysRevE.82.011301
- 683 Oppikofer, T., Jaboyedoff, M., & Kreusen H.-R. (2008). Collapse at the eastern Eiger flank in the  
684 Swiss Alps. *Nature Geoscience*, 8, 531-535.

- Pesci, A., Baldi, B., Bedin, A., Casula, G., Cenni, N., Fabris, M., Loddo, F., Mora, P., & Bacchetti, M. (2004). Digital elevation models for landslide evolution monitoring: application on two areas located in the Reno River Valley (Italy). *Annals of Geophysics*, 47, 1339-1353.
- Prokop, A., & Panholzer, H. (2009). Assessing the capability of terrestrial laser scanning for monitoring slow moving landslides. *Natural Hazards and Earth System Sciences*, 9, 1921-1928.
- Rohaly, J., Frigerio F., & Hart D. P. (2002). Reverse hierarchical PIV processing. *Measurement Science and Technology*, 13, 984-996.
- Squarzoni, C., Delacourt, C., & Allemand, P. (2005). Differential single-frequency GPS monitoring of the La Valette landslide (French Alps). *Engineering Geology*, 79, 215-229.
- Sturzenegger, M., & Stead, D. (2009). Close-range terrestrial digital photogrammetry and terrestrial laser scanning for discontinuity characterization on rock cuts. *Engineering Geology*, 106, 163-182.
- Tarchi, D., Casagli, N., Fanti, R., Leva, DD., Luzi, G., Pasuto, A., Pieraccini, M., & Silvano, S. (2003). Landslide monitoring by using ground-based SAR interferometry: an example of application to the Tessina landslide in Italy. *Engineering Geology*, 68, 15-30.
- Teza, G., Galgaro, A., Zaltron, N. & Genevois, R. (2007). Terrestrial laser scanner to detect landslide displacement fields: a new approach, *International Journal of Remote Sensing*, 28, 3425-3446.
- Teza, G., Pesci, A., Genevois, R., & Galgaro, A. (2008). Characterization of landslide ground surface kinematics from terrestrial laser scanning and strain field computation. *Geomorphology*, 97, 424— 437.
- Travelletti, J. & Malet, J-P (2011, in press). Characterization of the 3D geometry of flow-like landslides: a methodology based on the integration of multi-source data. *Submitted in Engineering Geology*.
- Wangensteen, B., Guomundsson, A., Eiken, T., Kääb, A., Farbrot, H., & Etzelmüller, B. (2006). Surface displacements and surface estimates for creeping slope landforms in Northern and Eastern Iceland using digital photogrammetry. *Geomorphology*, 80, 59-79.
- White, D. J., Take, W. A. & Bolton, M. D., (2003). Soil deformation measurement using particle image velocimetry (PIV) and photogrammetry. *Géotechnique*, 53, 619-631.

## Figures

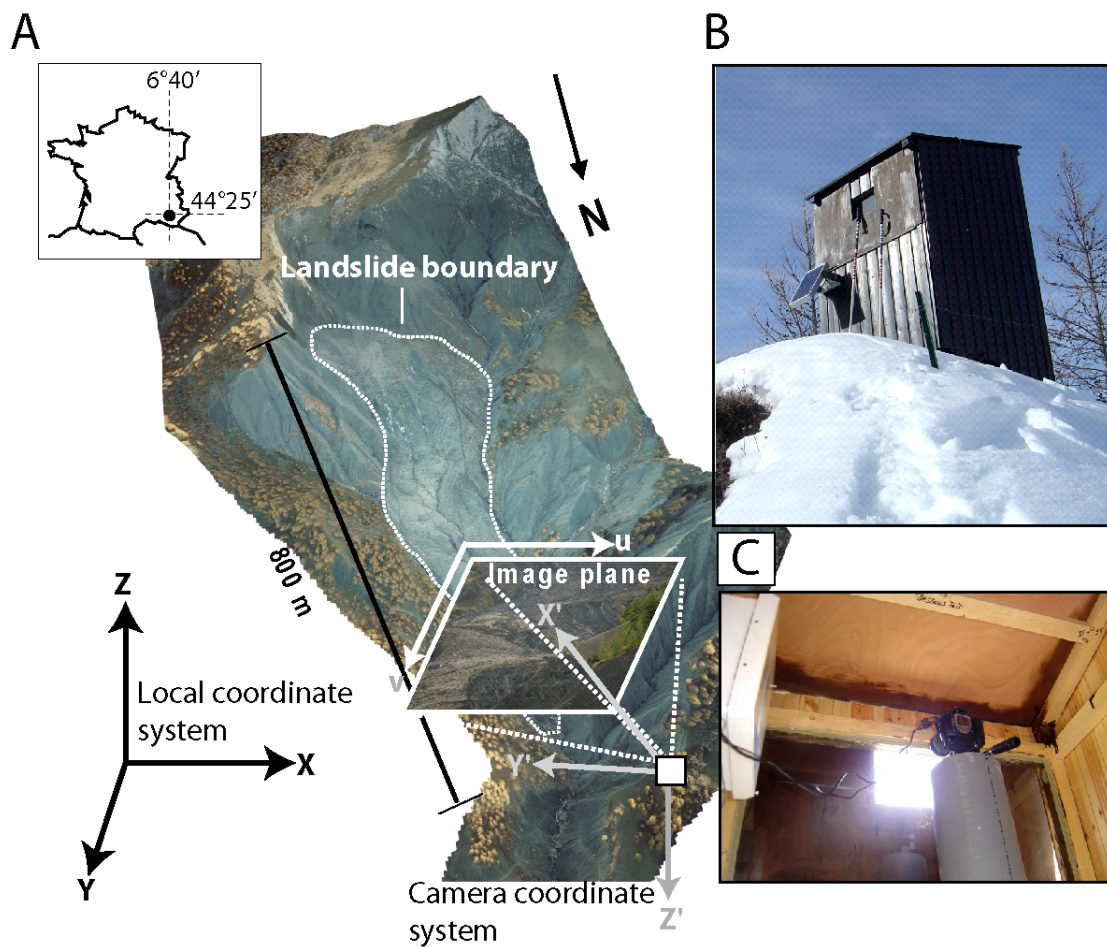


Fig. 1. (A) View of the Super-Sauze landslide towards the south with the different coordinate systems used in the georeferencing procedure. (B) Location of the camera monitoring system (C)



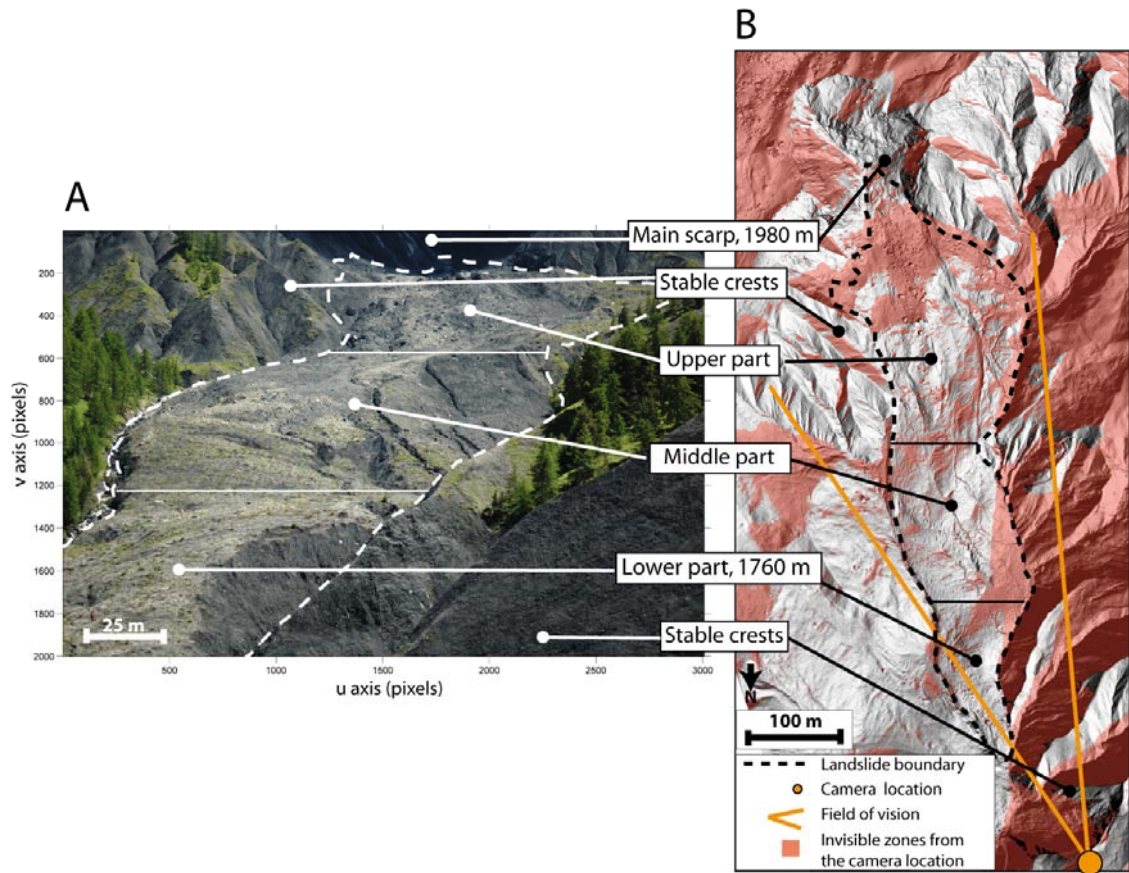


Fig. 2. Views of the landslide in the image geometry and in the local coordinate system (A) Image acquired by the monitoring system showing the different parts of the landslide from the camera location. (B) View of the landslide morphology in the local coordinate system on a shaded relief computed with a 0.25 m mesh DEM interpolated from airborne-LiDAR data sets acquired in July 2009. The invisible areas from the camera location are also shown.



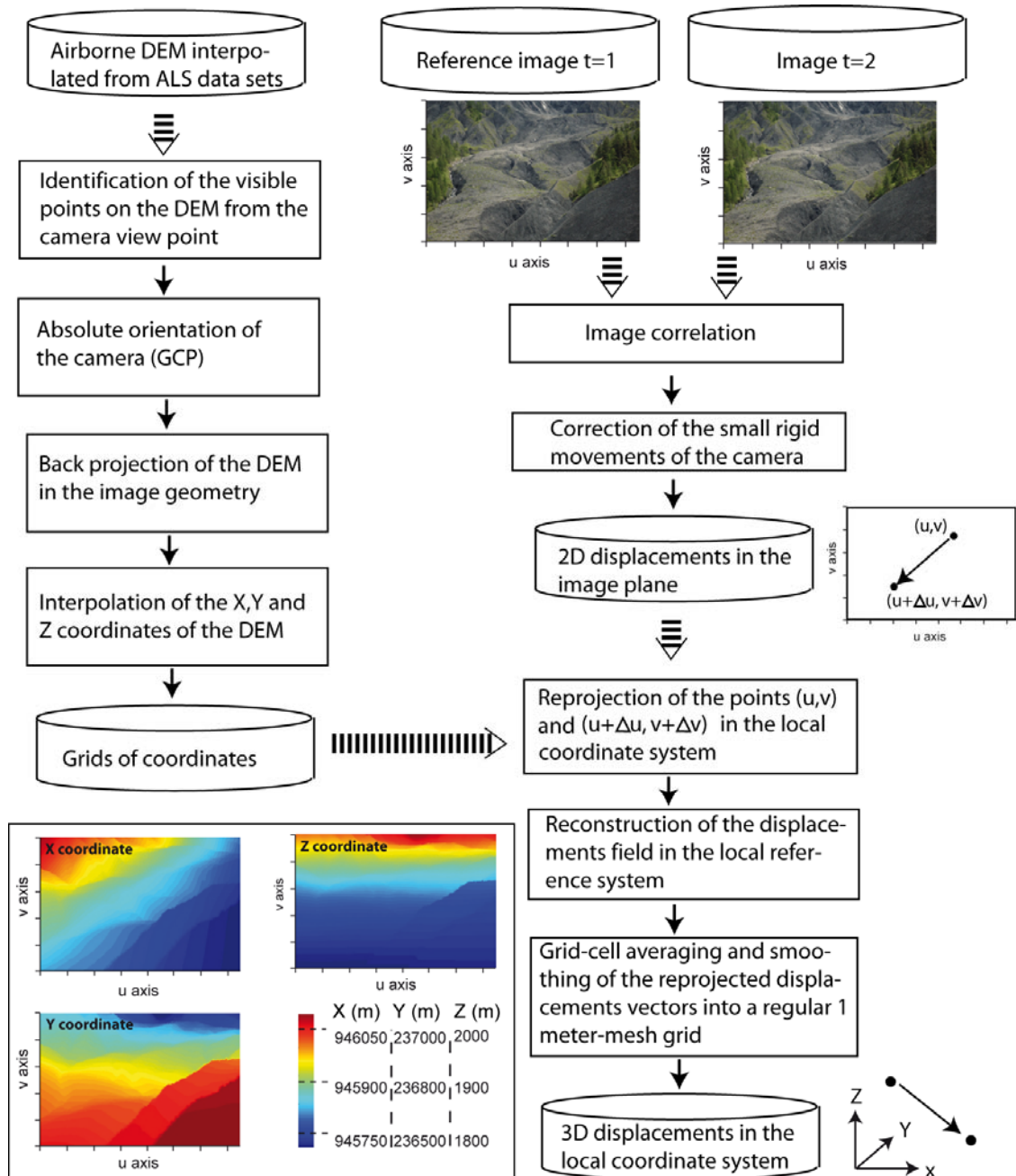


Fig 3. Flowchart of the methodology

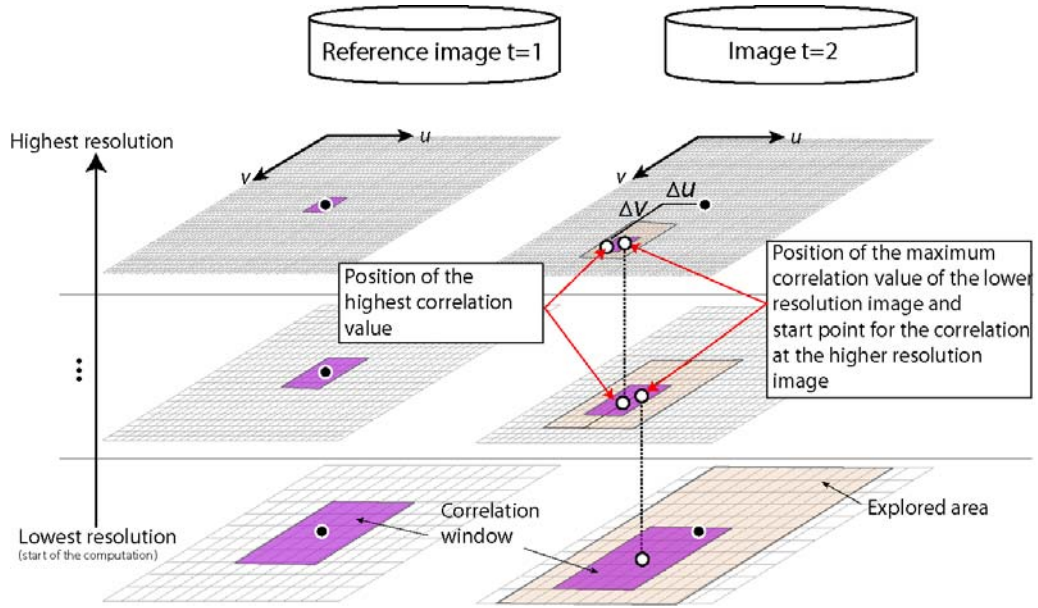


Fig. 4. Principle of the normalized hierarchical image correlation. The correlation computation starts from the lowest resolution to the highest resolution by keeping constant the size of the correlation window and the explored area, while their physical size is decreasing. At each higher resolution level, the explored area is centered on the pixel with the highest  $t$  correlation value of the previous resolution level. The estimate of the position of the maximum correlation value is thus increased.

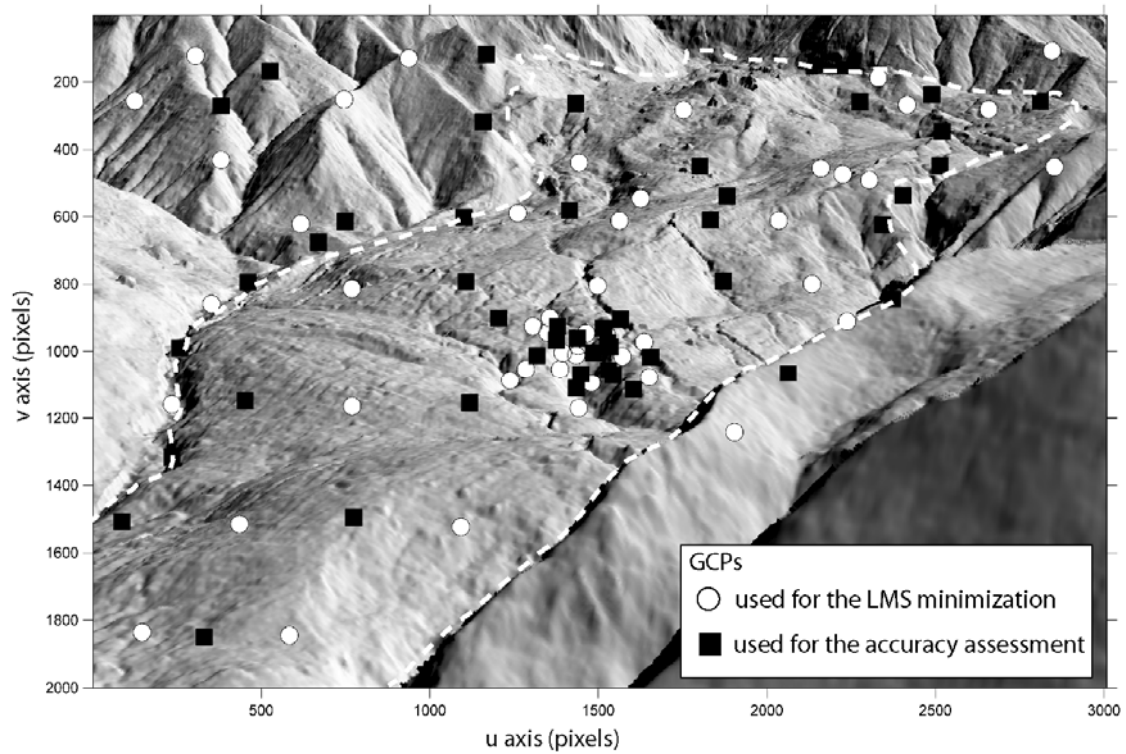


Fig.5. Location of the GCPs used for the Least Mean Square minimization (LMS) and for the accuracy analysis in a shaded relief image. The shaded relief image is produced by interpolating the shaded relief values of the DEM of 2009 projected in the image plane. This image is useful to visually check the quality of the back projection by comparison with a real image.

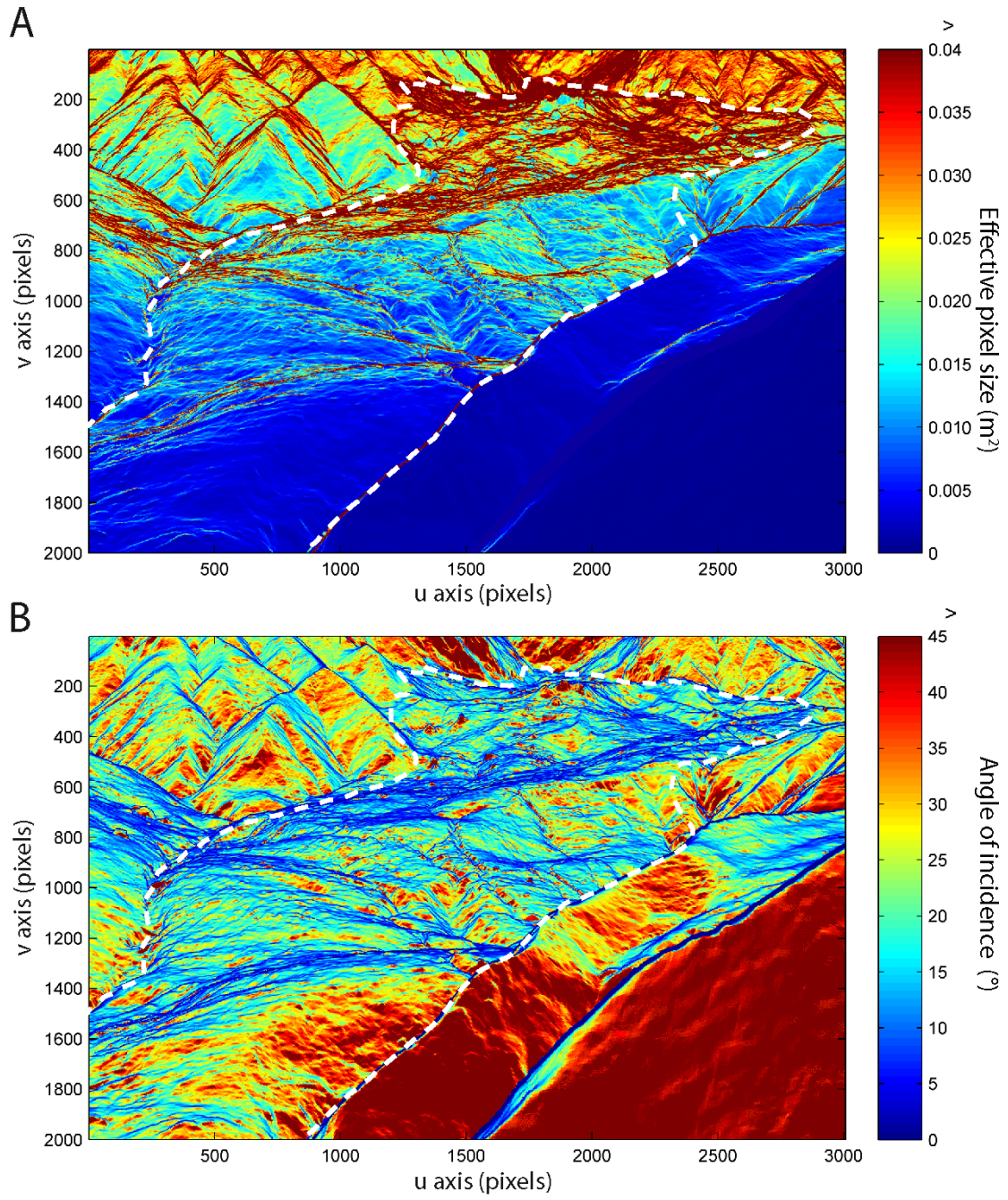


Fig. 6. Image resolution characteristics: (A) Effective pixel size in square meters (B) Angle of incidence in degrees. A low angle means that the line of sight is nearly tangential to the topography.

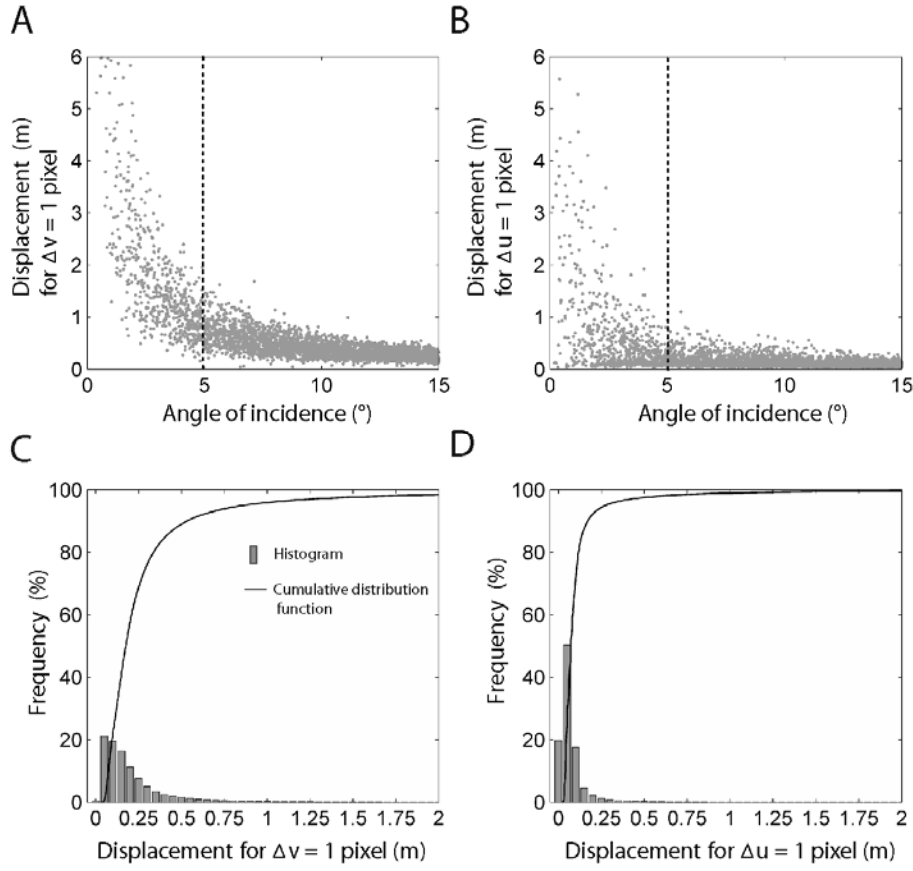


Fig. 7. Minimum metric displacement for pixel accuracy in v-axis (A) and u-axis (B) according to the angle of incidence. The sensitivity of metric displacements to small changes in u and v directions drastically increases for angle of incidence below  $5^\circ$ . (C) and (D) histograms and cumulative distribution function of the metric displacements resulting for 1 pixel displacement in v-axis and u-axis. 50% of the pixels in the image plane inside the landslide area shows a metric sensitivity less than 0.17 m for 1 pixel displacement in v-axis and 0.07 m in u-axis.



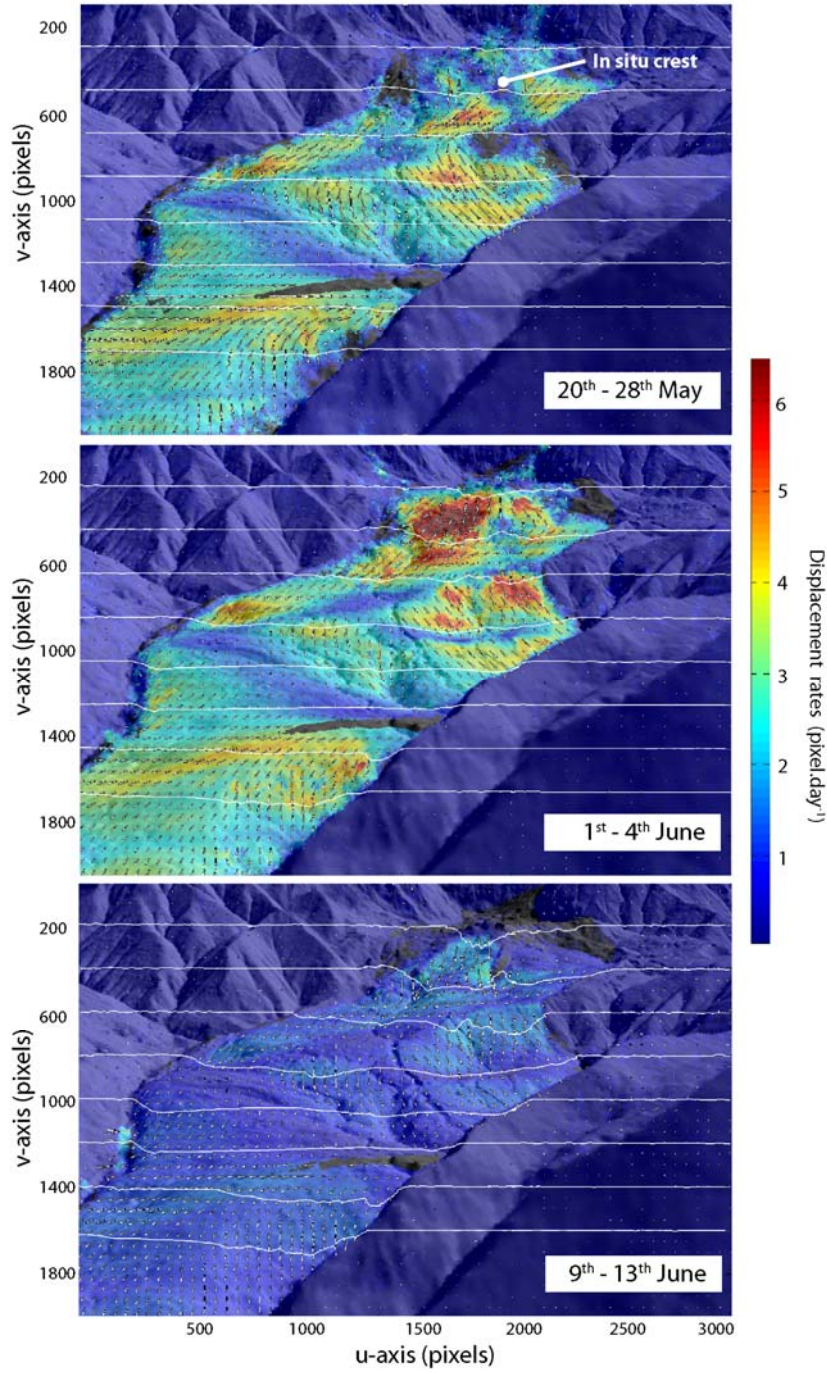


Fig. 8. Displacement rates amplitude (color) and displacement direction (arrows) in the image plane and cumulated displacements along 8 profiles crossing the landslide over the period the 20<sup>th</sup> May to the 25<sup>th</sup> June 2008. In order to highlight the displacement direction, the arrow length is normalized in each image.



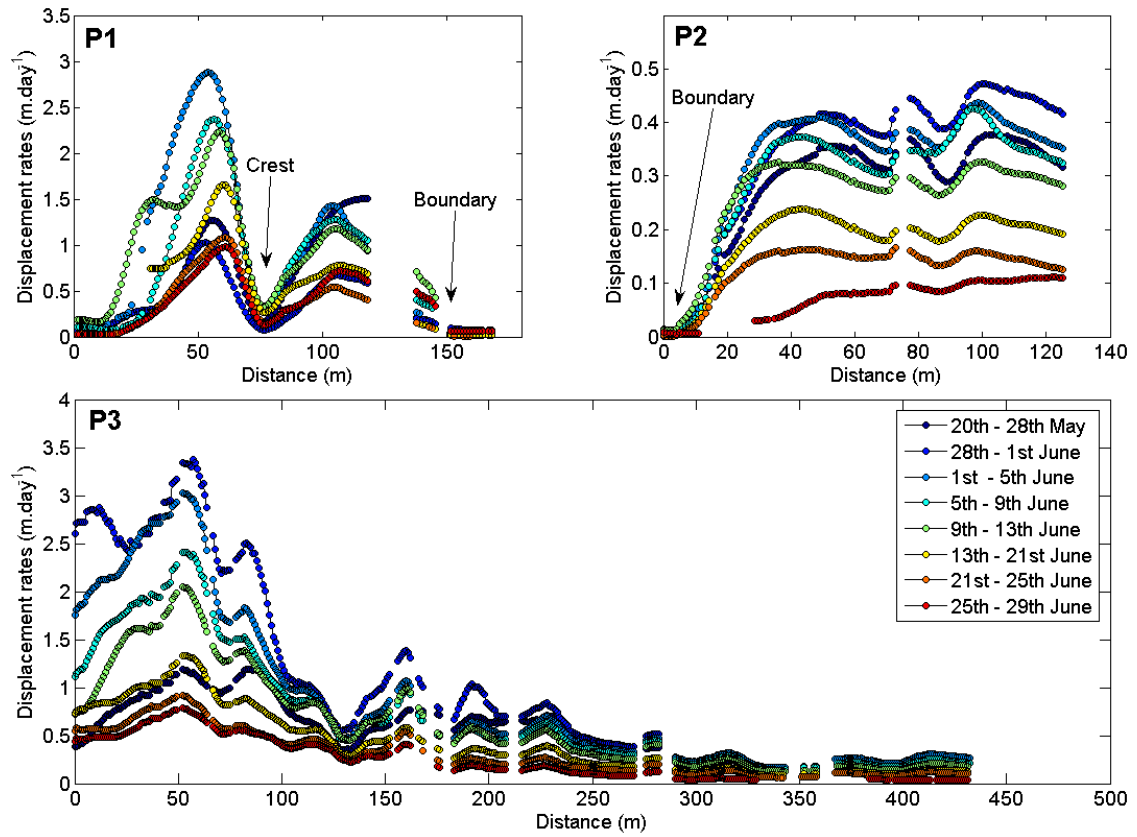


Fig. 10. Displacement rates profiles in the upper (P1), the medium (P2) and the lower (P3) part of the landslide. The location of the profiles is indicated in Fig. 9.



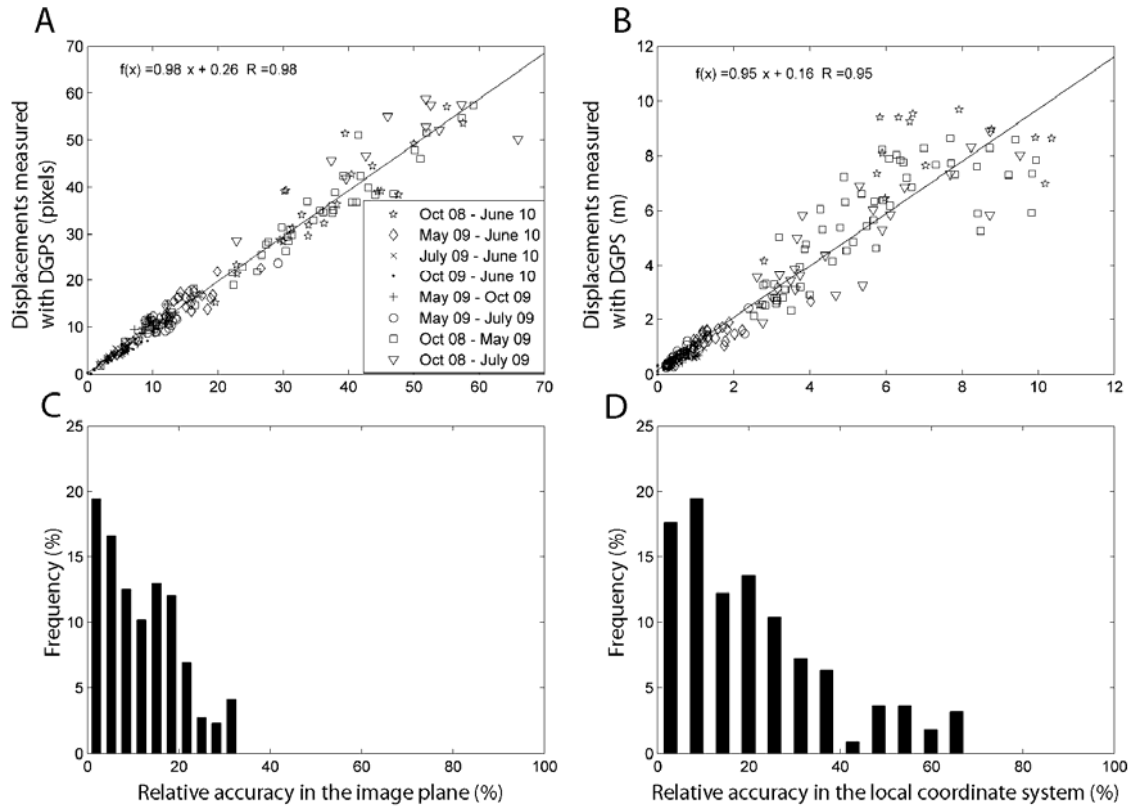


Fig. 11. Assessment of the accuracy of the Image Correlation technique. Relationships between the displacements observed by Image Correlation and the displacements observed by DGPS on sixty benchmarks in the image plane (A) and in the local coordinate system (B). Relative accuracy of the Image. Correlation technique in the images plane (C) and in the local coordinate system (D).

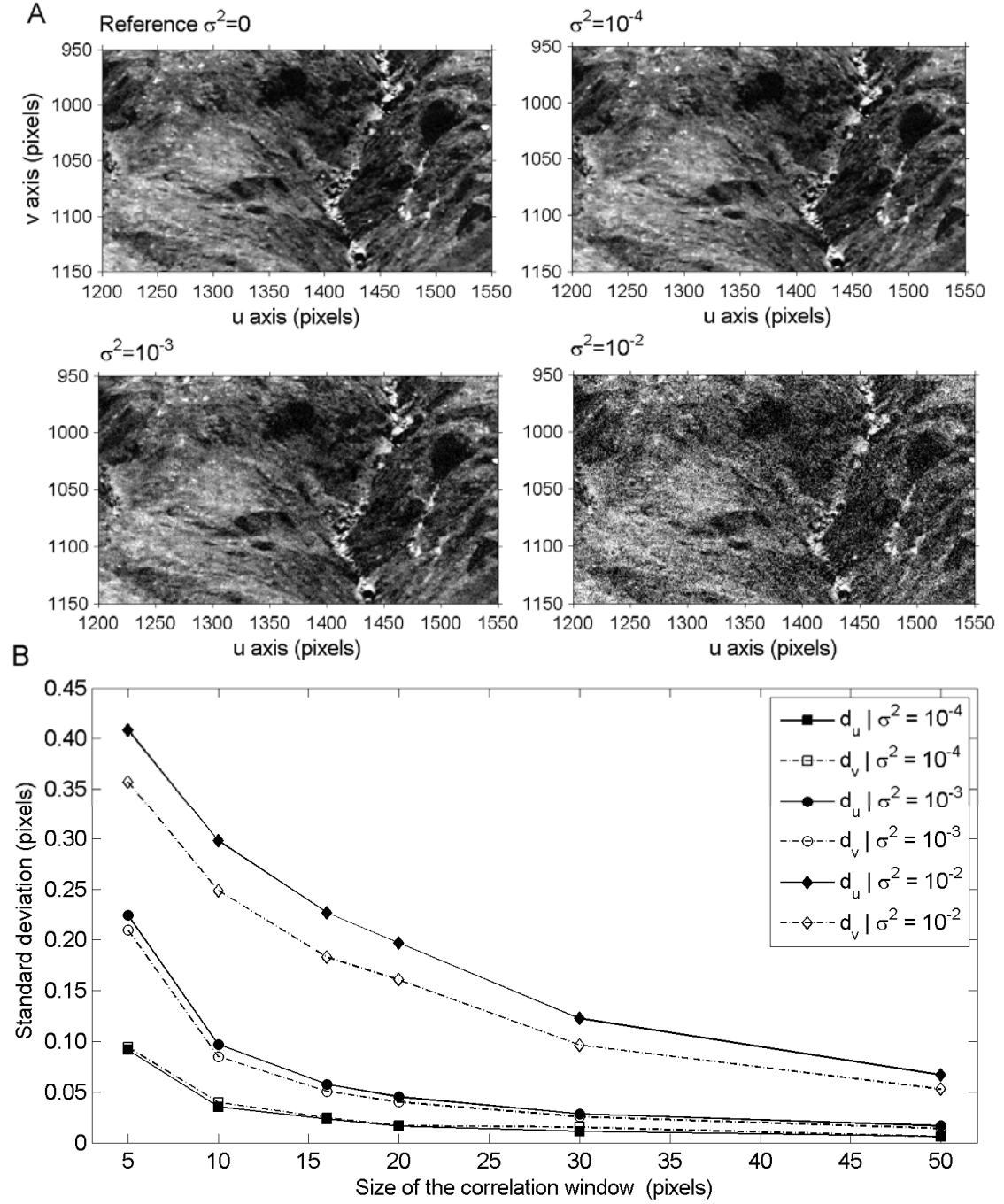


Fig. 12. Precision of the correlation algorithm. (A) Examples of different level of Gaussian noise created in the images of displacements (B) Precision of the hierarchical correlator in the  $u$  and  $v$  direction as a function of different levels of Gaussian noise ( $\sigma_n^2$ ) and different sizes of the correlation window.

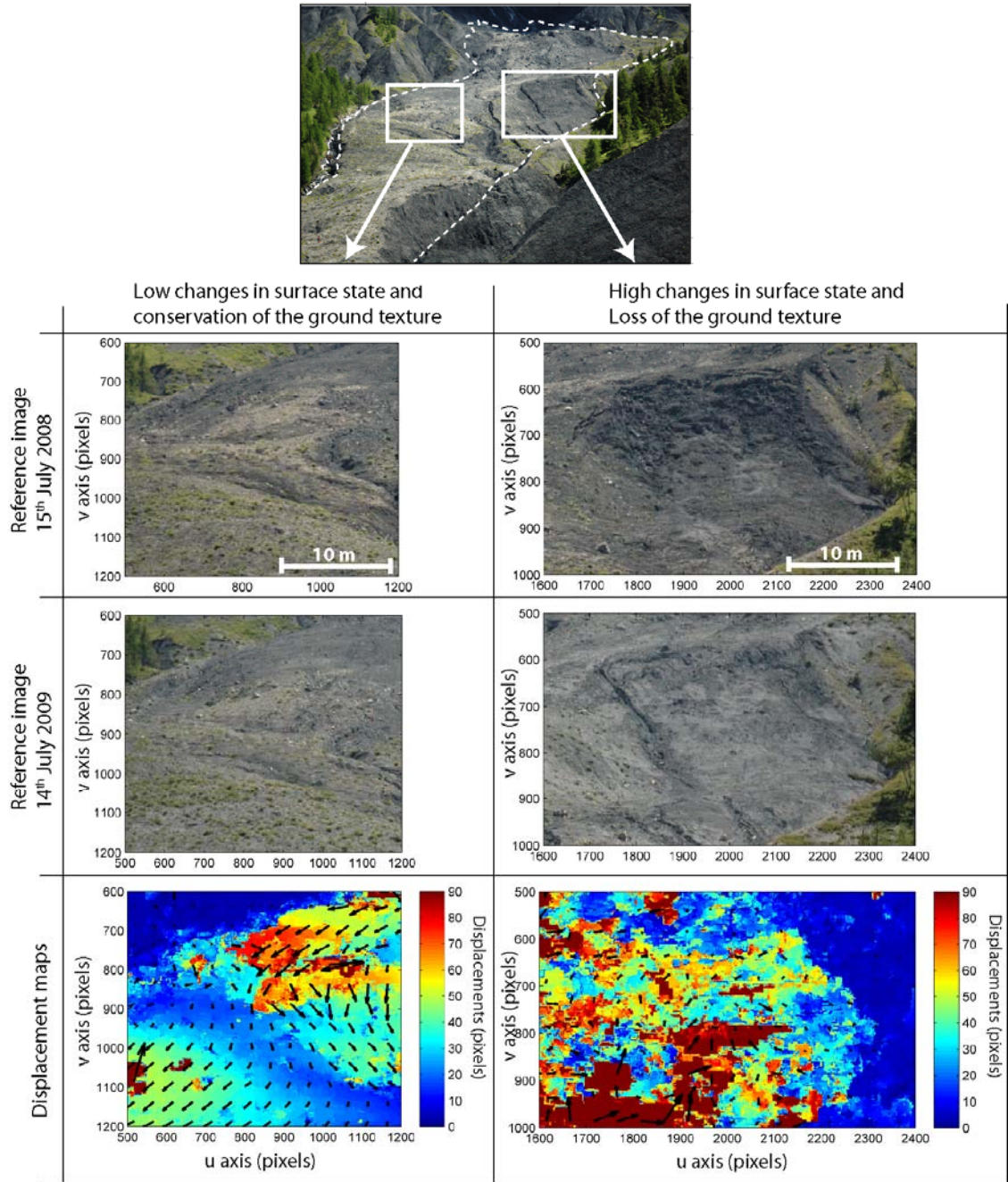


Fig. 13. Example of results for the correlation of two images acquired with one year interval (15<sup>th</sup> July 2008-14<sup>th</sup> July 2009), at the same solar time and clear sky conditions. Depending on the location in the landslide, some areas conserved their texture while others areas affected by strong weathering and ground deformation (loading of the snow and landslide displacement) display a totally different ground texture. The incoherency of the displacements is therefore clearly identifiable (inhomogeneous amplitude and direction of the displacement vectors).

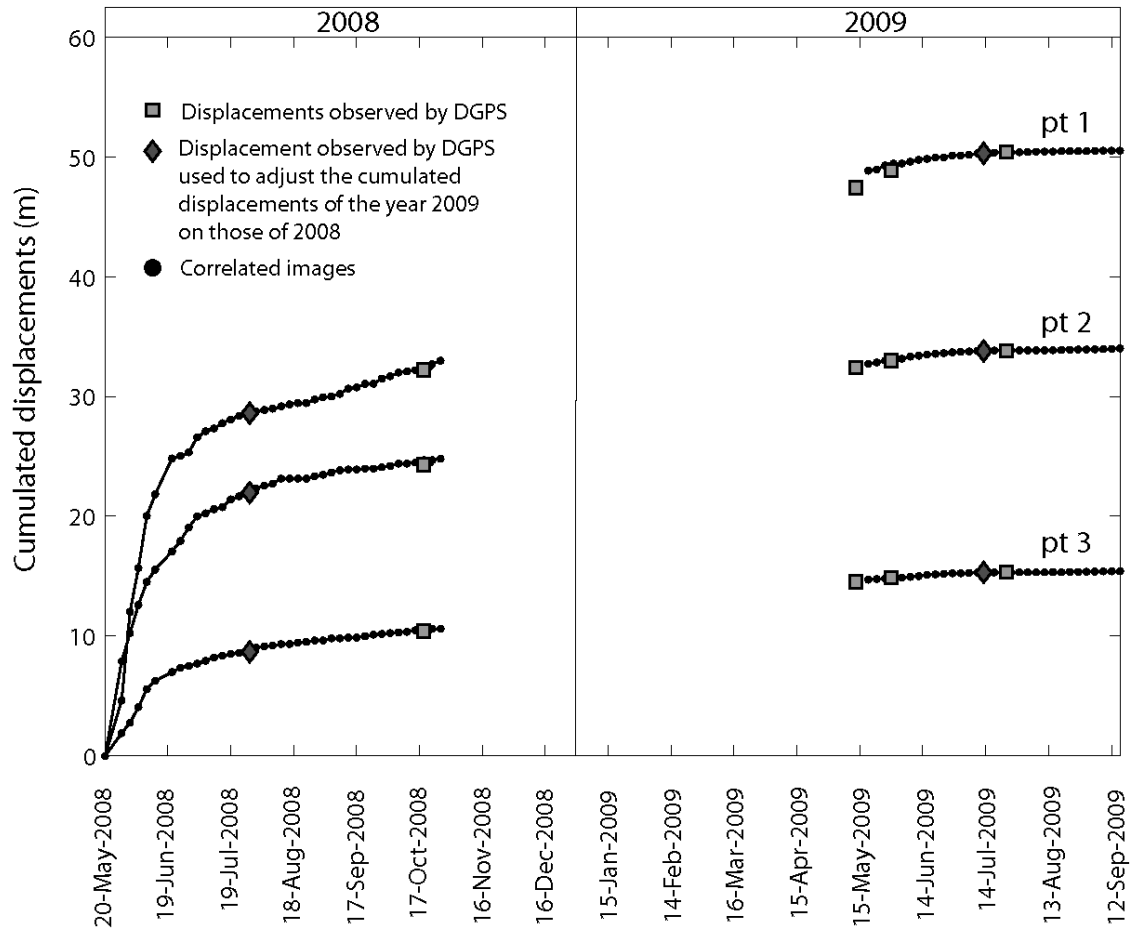


Fig. 14. Cumulated displacements at three locations in the upper (pt1), middle (pt2) and lower (pt3) parts of the landslide. The location of the points is indicated in Fig. 9. The cumulated displacements of the year 2009 are adjusted on those of 2008 using GCPs measured with DGPS at the vicinity of the points pt1, pt2 and pt3.

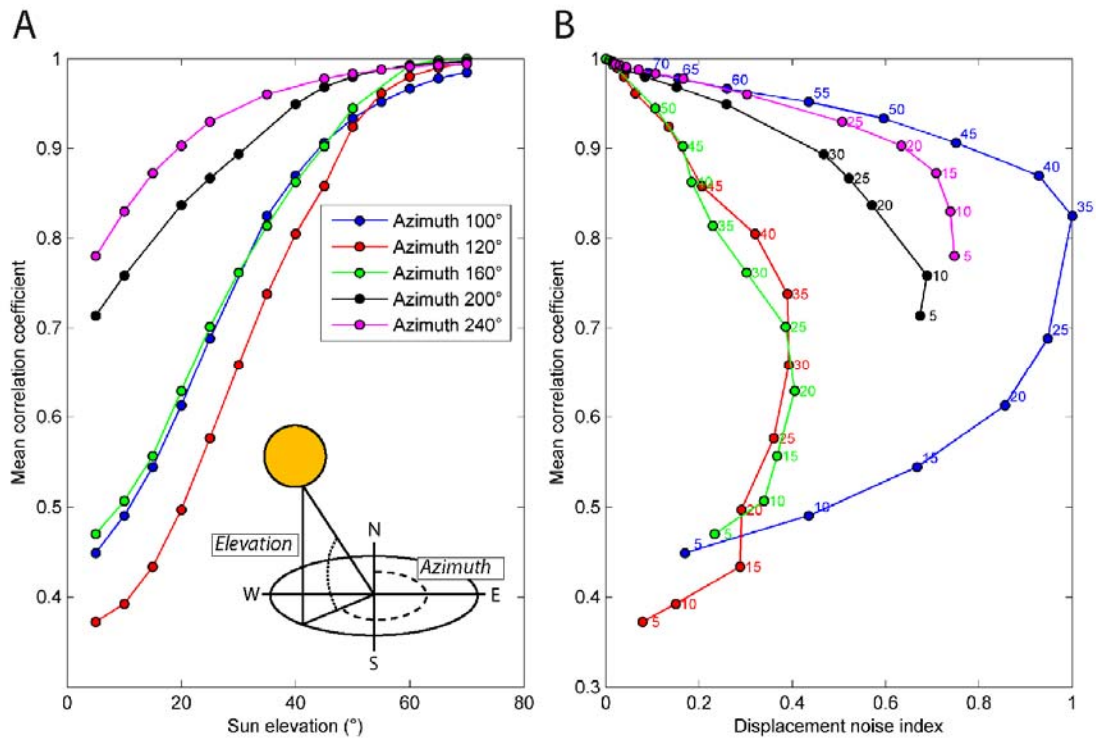


Fig. 15. Results of the correlation on the synthetic shaded relief images. (A) Influence of illumination conditions as a function of the sun elevation and azimuth on the mean correlation coefficient. (B) Relationship between displacement noise index and correlation coefficient. The values near the dots correspond to the sun elevation angles.

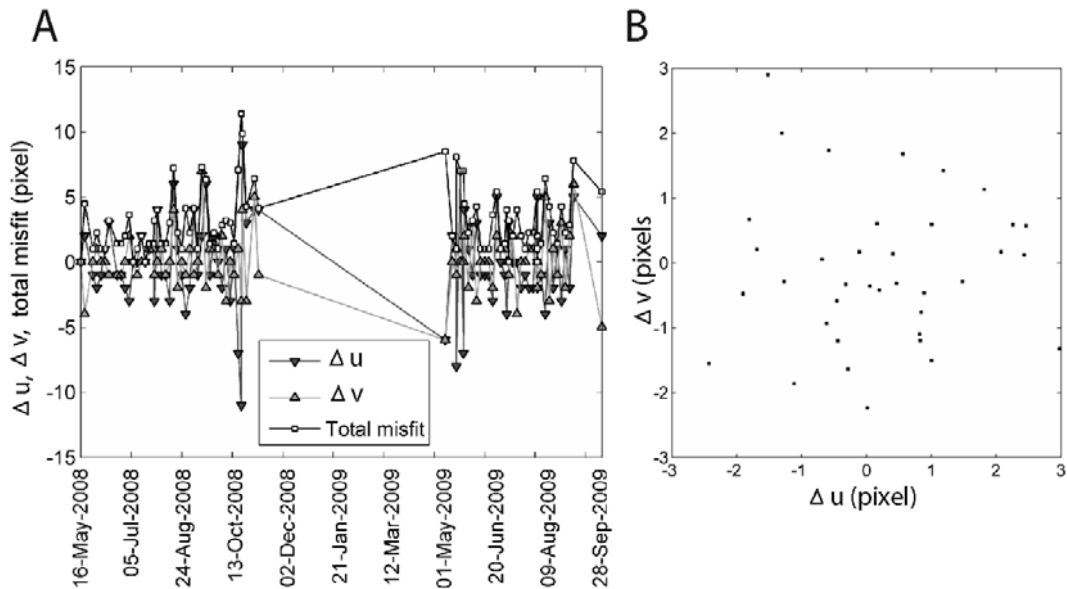


Fig. 16. Assessment of the accuracy of the camera orientation (A) Average homogenous components due to slight movement of the camera. (B) Residual  $\Delta u$  and  $\Delta v$  misfits between projected and observed GCPs after the least square minimization.

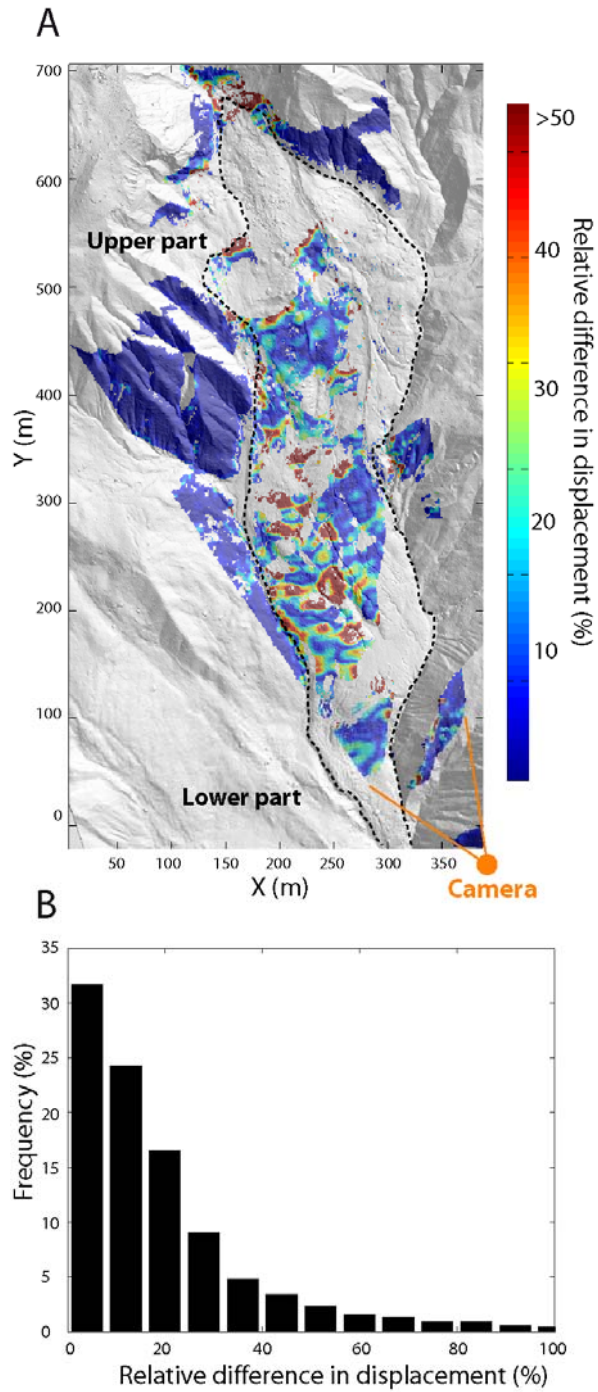


Fig. 17. Effect of the DEM on the ortho-rectification of the displacement field. (A) relative difference between the displacement field of the 1<sup>st</sup> June orthorectified with a DEM of 2007 and a DEM of 2009. (B) Histogram of the relative differences.

## Tables

Table 1. Relative advantages and disadvantages for GB-InSAR, TLS and TOP

Techniques	Relative advantages	Relative disadvantages
GB-InSAR	<p>High data accuracy possible (millimetric accuracy)</p> <p>Monitoring during night and any type of weather conditions</p> <p>Atmospheric effects can be corrected (permanent scatterers)</p> <p>Potential for high level of automation in acquisition and post-processing</p>	<p>Requires large initial investment if buying</p> <p>Skilled crew required for operation</p> <p>Displacement along line of sight</p> <p>Fails in detecting large and rapid displacements (signal decorrelation)</p> <p>Sensitive to changes in acquisition geometry and surface state variations</p>
TLS	<p>High data accuracy possible 1-4 cm (at 100 m range); 30 cm (at 1000 m range)</p> <p>Provide an easily understandable image</p> <p>Potential for high level of automation in acquisition</p>	<p>Requires large initial investment if buying</p> <p>Skilled crew required for operation</p> <p>Computation of the true 3D displacements require specific algorithms optimized for calculations on large 3D point clouds</p> <p>Large amount of computational resources for the spatial data visualization</p> <p>Automated data post-processing difficult</p>
TOP	<p>High data accuracy possible from millimeters to a few centimeters at 100 m range</p> <p>Provide an easily understandable image</p> <p>Low initial cost and operating cost</p> <p>Low energy supply (passive sensors)</p> <p>Potential for high level of automation in acquisition and post-processing</p> <p>Simple camera calibration processes available</p> <p>Simple matching algorithms available to produce DEMs and to compute 2D displacement fields</p>	<p>Adverse weather and illumination changes affects image quality</p> <p>Not operating during the night</p> <p>Very Sensitive to changes in acquisition geometry and surface state variations</p> <p>Ortho-rectification using accurate DEM is necessary for quantitative analysis</p> <p>Ground control points necessary for camera calibration</p>

Table 2. Camera acquisitions characteristics

Type of Camera	Single-lens reflex digital camera
Effective Pixels	6.1 million
Image Sensor	RGB CCD, 23.7 x 15.6 mm
Image Size	3008 x 2000
Sensitivity	400 iso
Focal length	52 mm
Shutter speed	1/800
Storage Media	CompactFlash™ (CF) Card
Storage System	NEF (RAW)

Table 3. Quantity of interpretable displacement values in summer and in autumn after filtering according to the location in the landslide (Fig. 2)

	Total		1. Correlation coefficient > 0.6		2. Downslope displacements		3. Displacements in visible areas	
	Absolute quantity of values (-)	Relative quantity of values (%)	Absolute quantity of values (-)	Relative quantity of values (%)	Absolute quantity of values (-)	Relative quantity of values (%)	Absolute quantity of values (-)	Relative quantity of values (%)
<b>23 July - 27 July 2008</b>								
Upper part	210637	100	197139	93.6	164275	78.0	161221	76.5
Middle part	24821	100	23612	95.1	23266	93.7	22343	90.0
Lower part	61979	100	61255	98.8	59989	96.8	57801	93.3
Whole landslide	297437	100	282006	94.8	247530	83.2	241365	81.1
<b>19 Oct. - 23 Oct. 2008</b>								
Upper part	210637	100	183570	87.2	82149	39.0	74798	35.5
Middle part	24821	100	22847	92.1	20751	83.6	18672	75.2
Lower part	61979	100	61762	99.7	60019	96.8	57510	92.8
Whole landslide	297437	100	268179	90.2	162919	60.4	150980	50.8

Table 4. Mean  $\mu$  and standard deviation  $\sigma$  of the absolute accuracy for the projection in the image plane and the back-projection in the local coordinate system

Image plane (n=40)	$\mu$ (pixels)	$\sigma$ (pixels)
u	0.20	1.59
v	-0.08	1.51
Local coordinate system (n=11)	$\mu$ (m)	$\sigma$ (m)
X	0.07	0.41
Y	-0.13	0.53
Z	0.01	0.29



## **Figure captions**

Fig. 1. Overview of the Super-Sauze mudslide (South French Alps). (A) Monitoring system by terrestrial optical photography. (B) Image acquired by the monitoring system presenting the different parts of the landslide from the camera location. (C) View of the landslide morphology in the local coordinate system on a shaded relief computed with a 0.25 m resolution DEM interpolated from airborne-LiDAR data acquired in July 2009. The invisible areas from the camera location are indicated.

Fig 2. Flowchart of the methodology

Fig. 3. Principle of the normalized hierarchical image correlation.

Fig.4. Location of the GCPs used for the Least Mean Square minimization (LMS) and for the accuracy analysis on a shaded relief image. The shaded relief image is produced by interpolating the shaded relief values of the ALS DEM of 2009 projected in the image plane.

Fig. 5. Characteristics of the images: (A) Effective pixel size calculated with the ALS DEM of 2009 projected in the image geometry (in  $m^2$ ); (B) Angle of incidence (in degrees).

Fig. 6. Displacement rates amplitude (color) and direction (arrows) in the image plane and cumulated displacements along eight profiles crossing the landslide over the period 20 May-25 June 2008. In order to highlight the displacement direction, the arrow length is normalized for each image.

Fig. 7. Displacement rates map for the period 1-4 June 2008. The profiles P1, P2 and P3 refer to Fig. 8 and the locations pt 1, pt 2 and pt 3 refer to Fig. 12.

Fig. 8. Profiles of displacement rates in the upper (P1), middle (P2) and lower (P3) parts of the landslide. The location of the profiles is indicated in Fig. 7.

Fig. 9. Assessment of the accuracy of the Image Correlation technique. Relationships between the displacements observed by Image Correlation and the displacements measured by dGPS on sixty benchmarks in the image plane (A) and in the local coordinate system (B). Relative accuracy of the Image Correlation technique in the image plane (C) and in the local coordinate system (D).

Fig. 10. Precision of the correlation algorithm. (A) Examples of different level of Gaussian noise introduced in the images; (B) Precision of the hierarchical correlator in the  $u$  and  $v$  direction as a function of different levels of Gaussian noise ( $\sigma_n^2$ ) and different sizes of the correlation window.

Fig. 11. Example of results for the correlation of two images acquired with one year interval (15 July 2008-14 July 2009), at the same solar time and with clear sky conditions. The incoherency of the displacements are clearly identifiable due to strong surface texture changes (inhomogeneous amplitude and direction of the displacement vectors).

Fig. 12. Cumulated displacements at three locations in the upper (pt1), middle (pt2) and lower (pt3) parts of the landslide. The location of the points is indicated in Fig. 7.

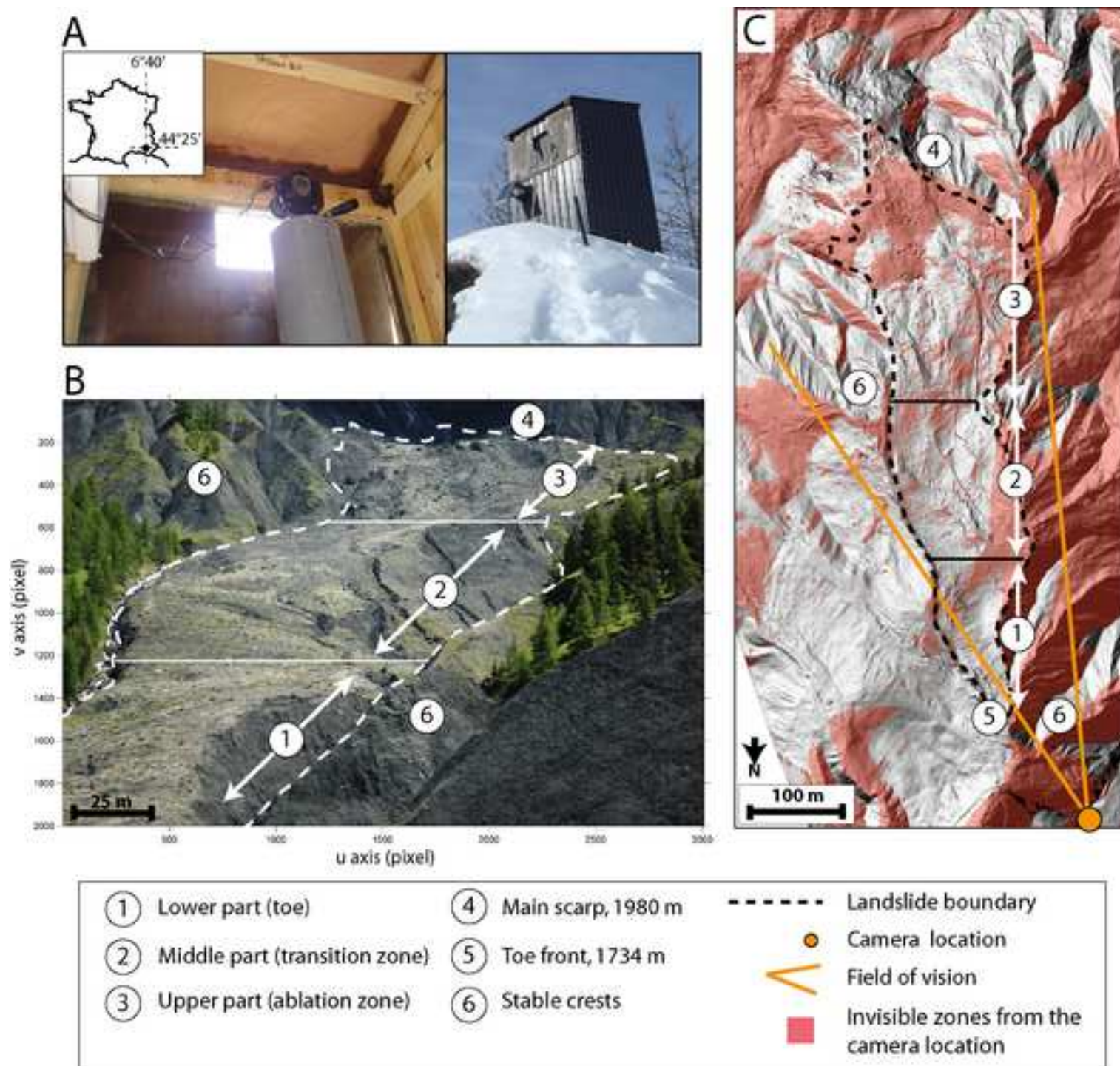
Fig. 13. Influence of illumination conditions as a function of the sun elevation and azimuth on the mean correlation coefficient.

Fig. 14. Assessment of the accuracy of the camera orientation. (A) Average homogenous components due to slight movement of the camera. (B) Residual  $\Delta u$  and  $\Delta v$  misfits between projected and observed GCPs after the least square minimization.

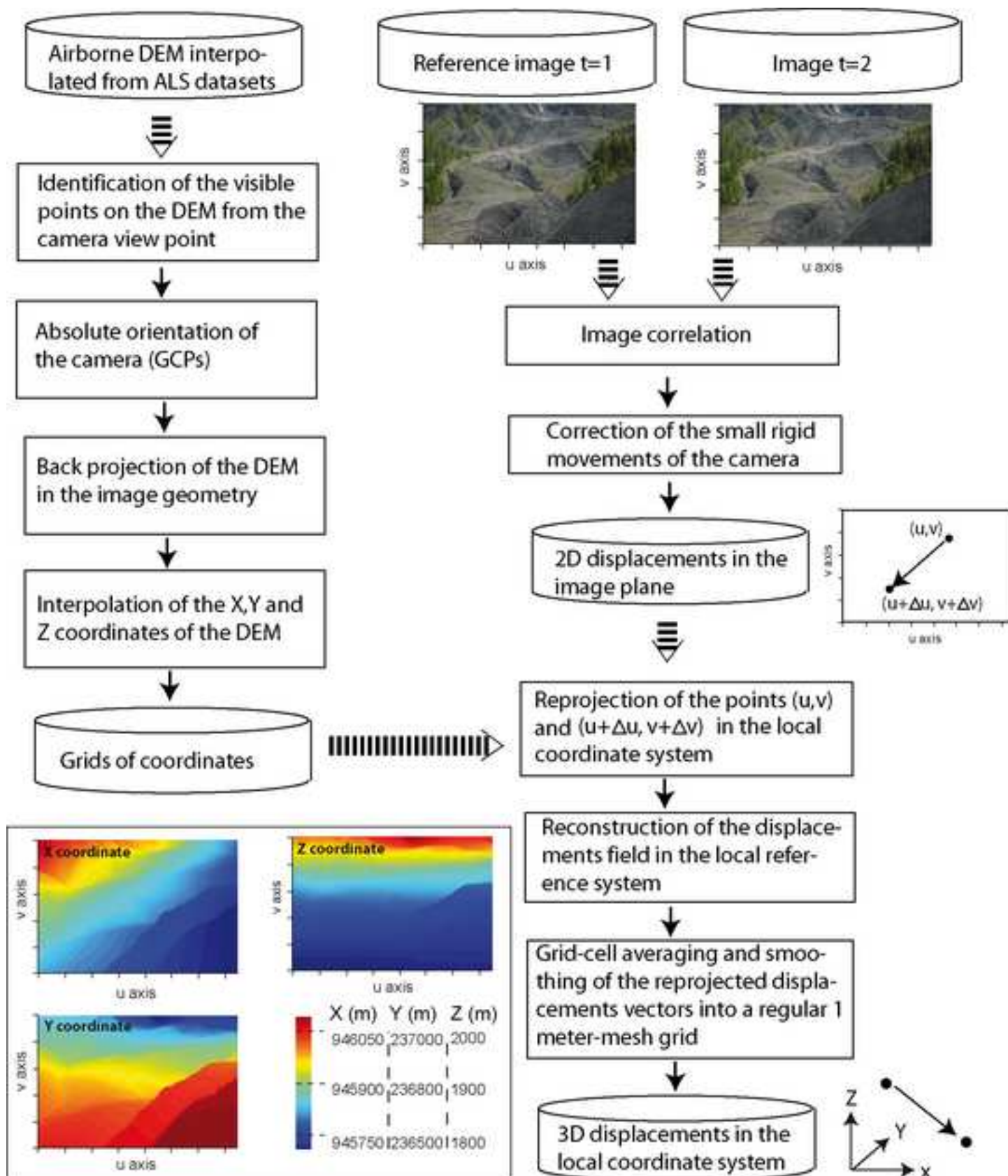
Fig. 15. Influence of the DEM on the orthorectification of the displacement field. (A) Relative difference between the displacement field of the 1<sup>st</sup> - 4<sup>th</sup> of June orthorectified with a DEM of 2007 and a DEM of 2009. (B) Histogram of the relative differences.

Figure(s)

[Click here to download high resolution image](#)



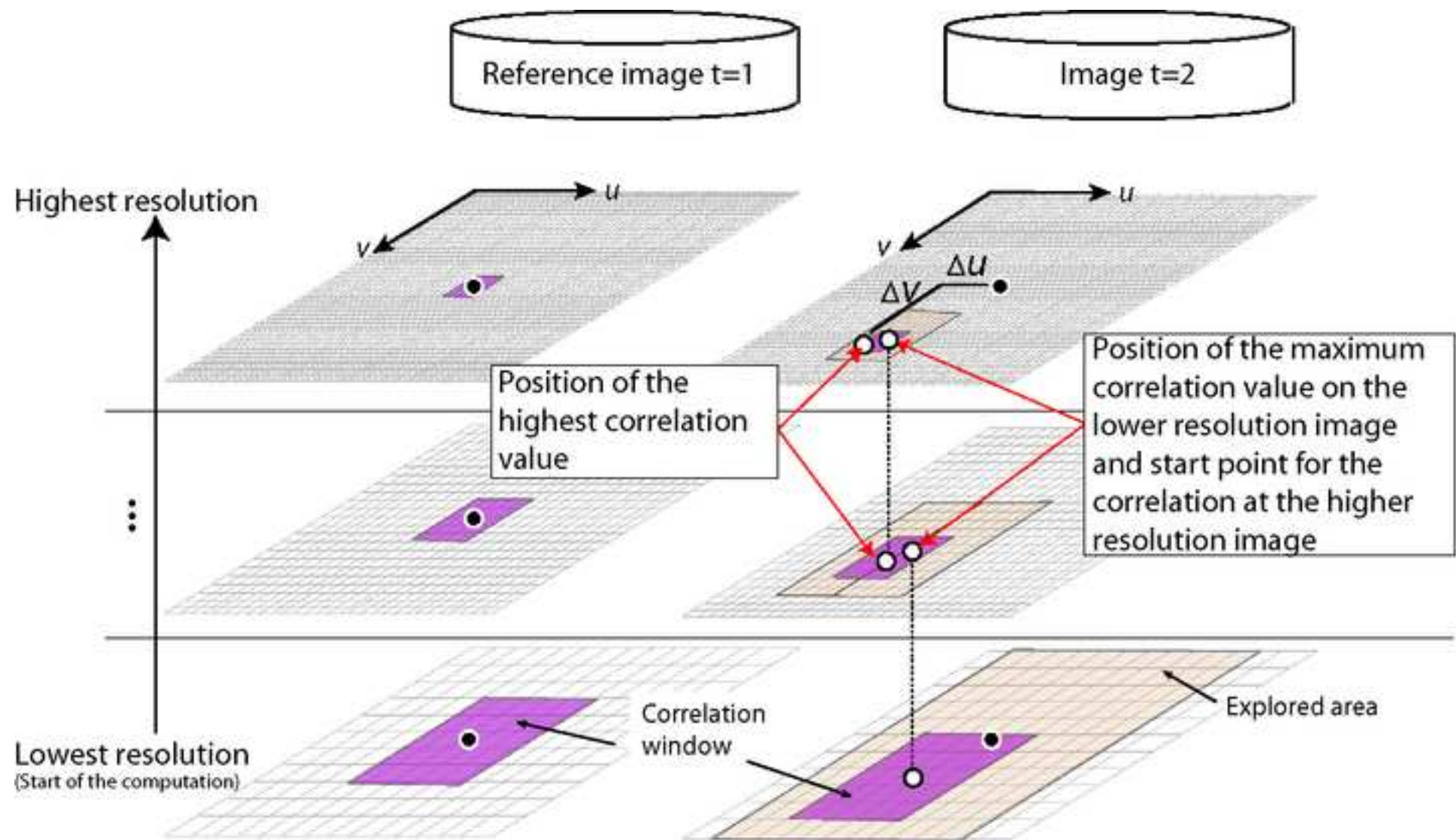
Figure(s)  
[Click here to download high resolution image](#)





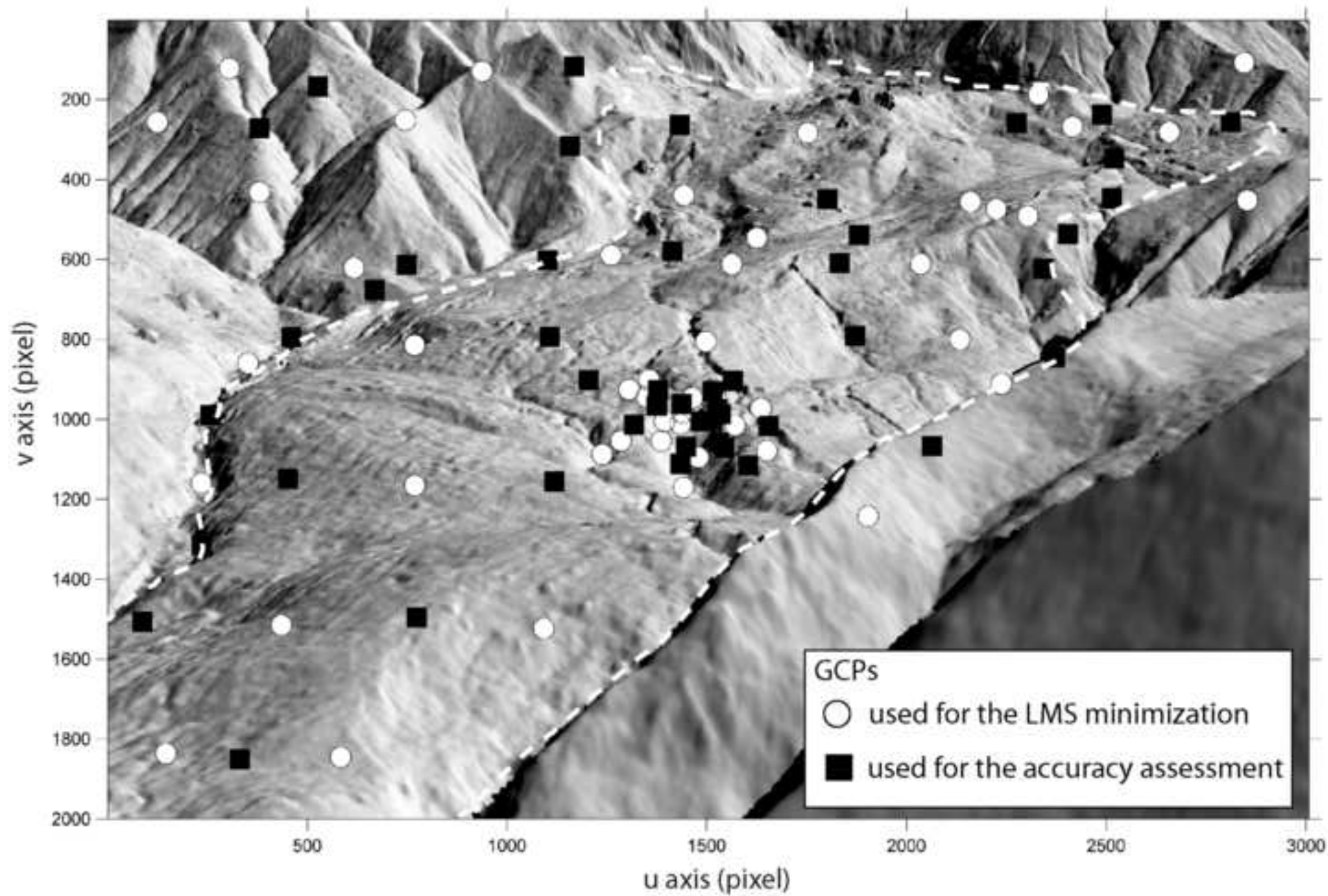
Figure(s)

[Click here to download high resolution image](#)



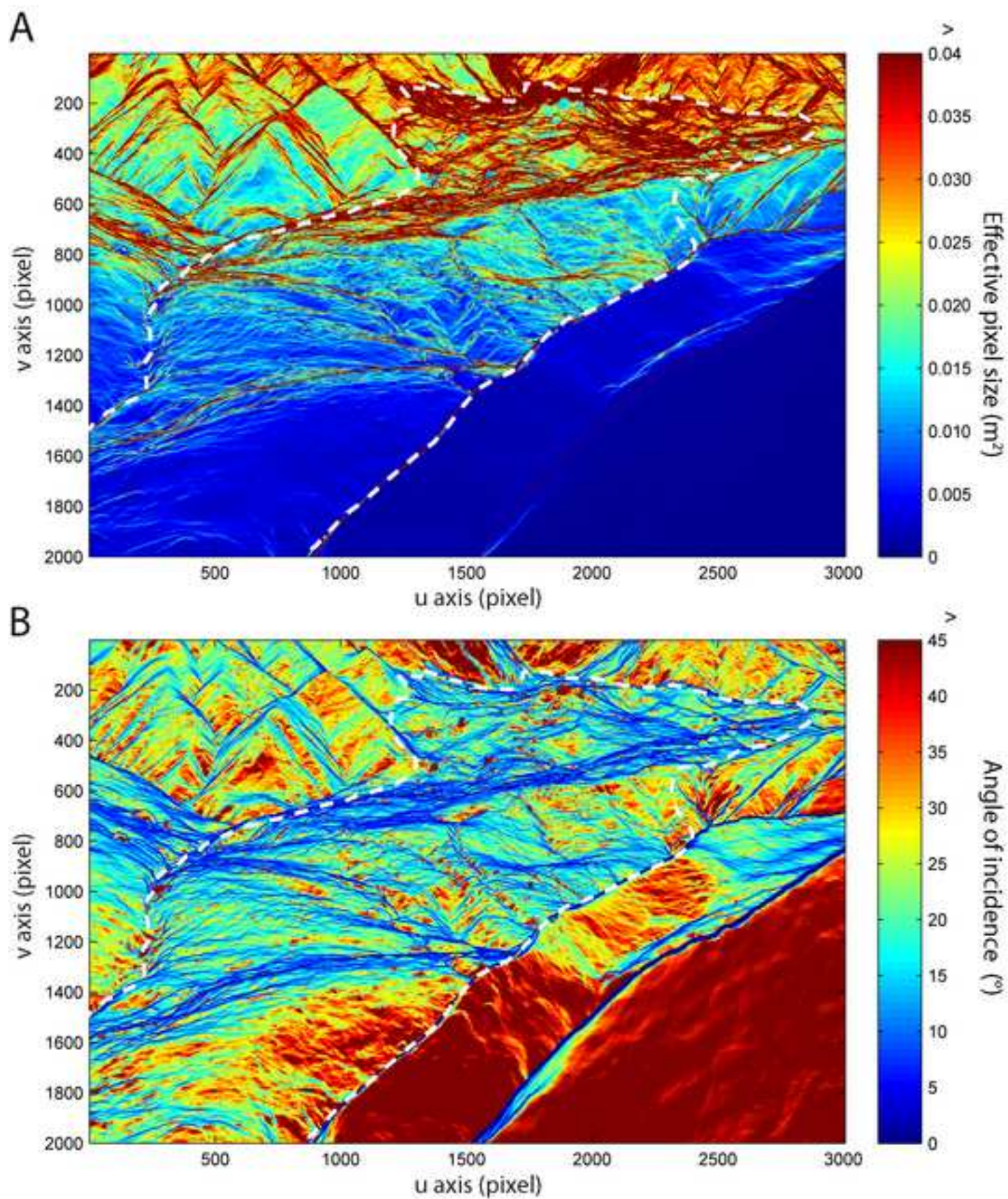
Figure(s)

[Click here to download high resolution image](#)



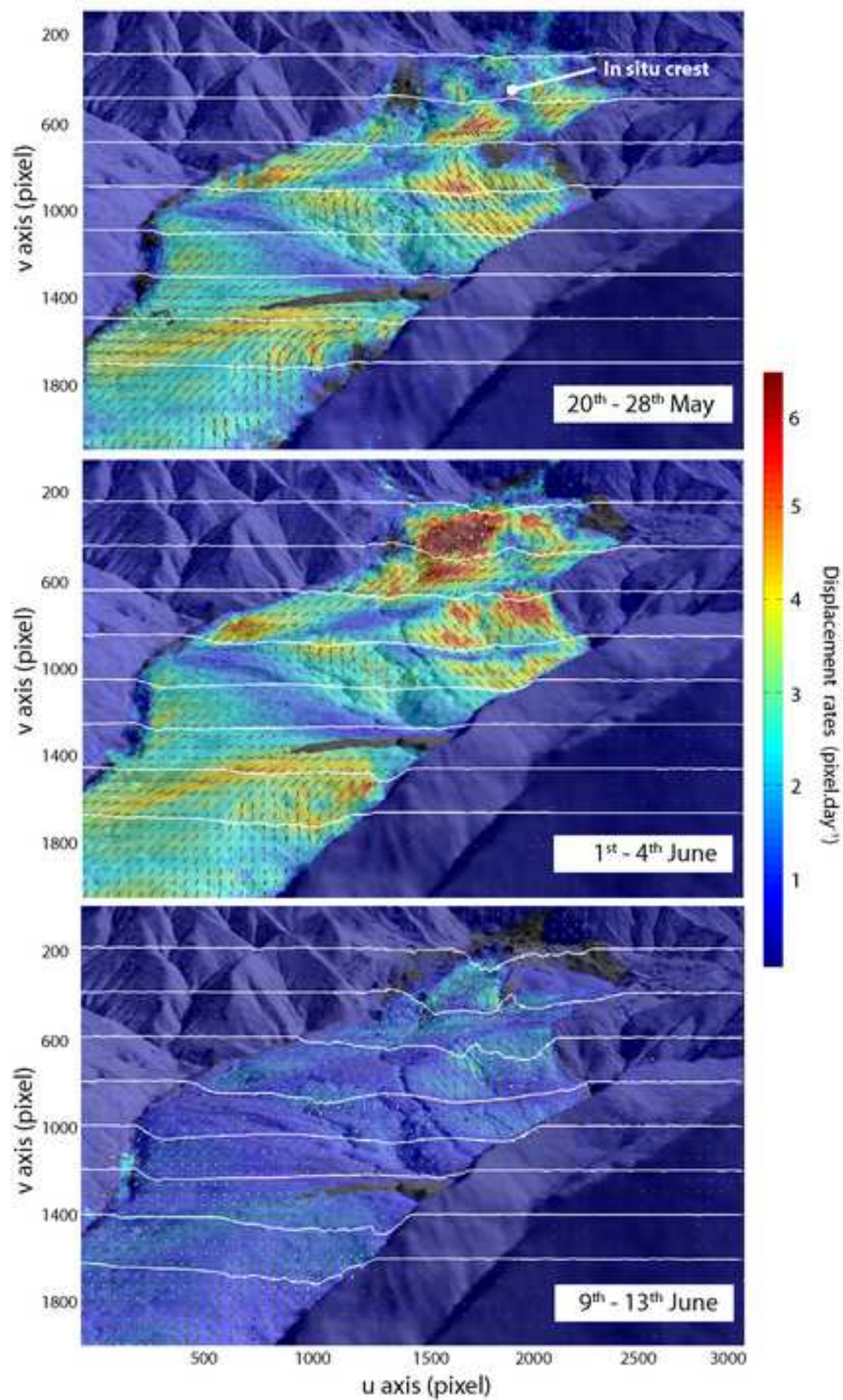


Figure(s)  
[Click here to download high resolution image](#)



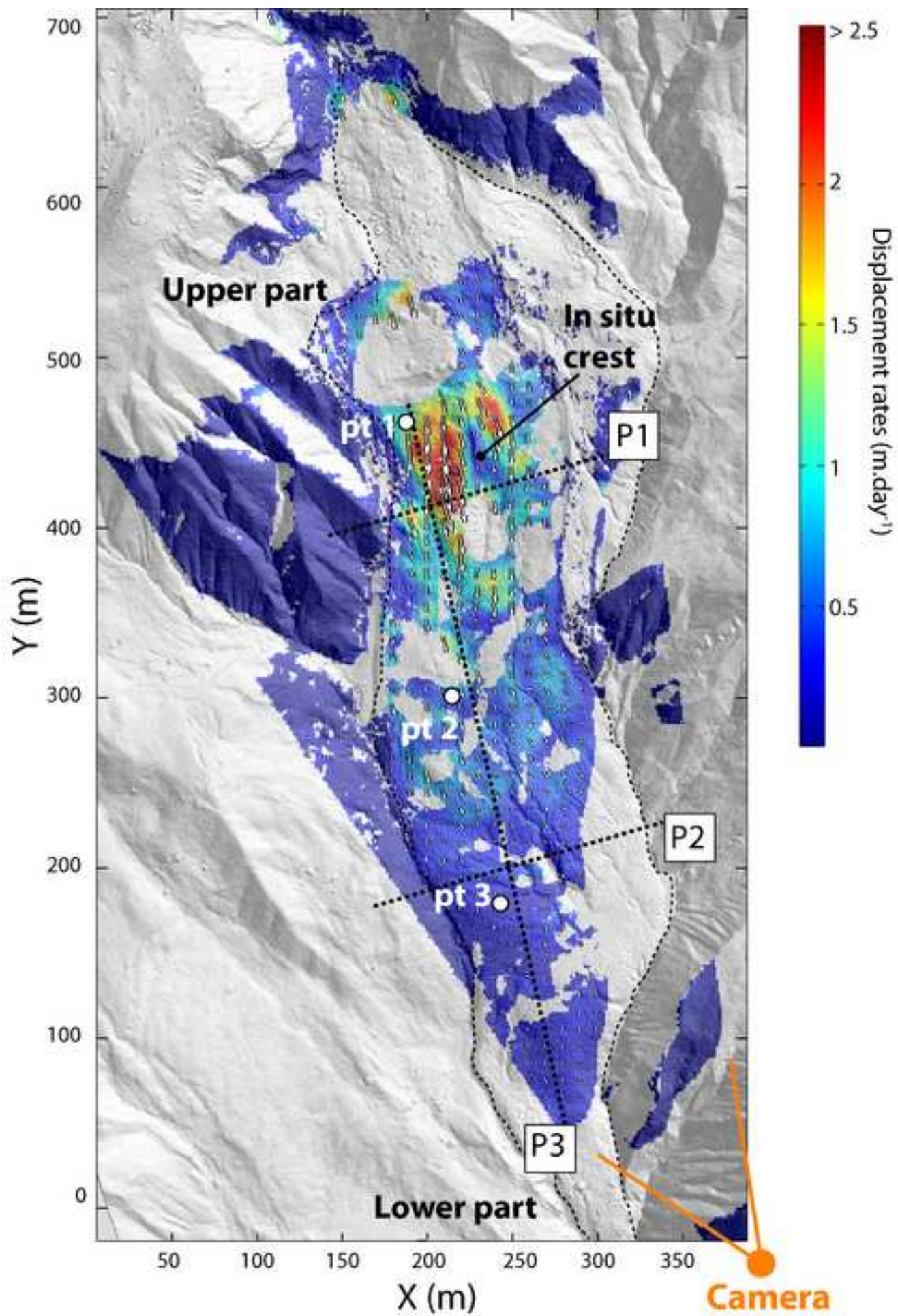


Figure(s)  
[Click here to download high resolution image](#)



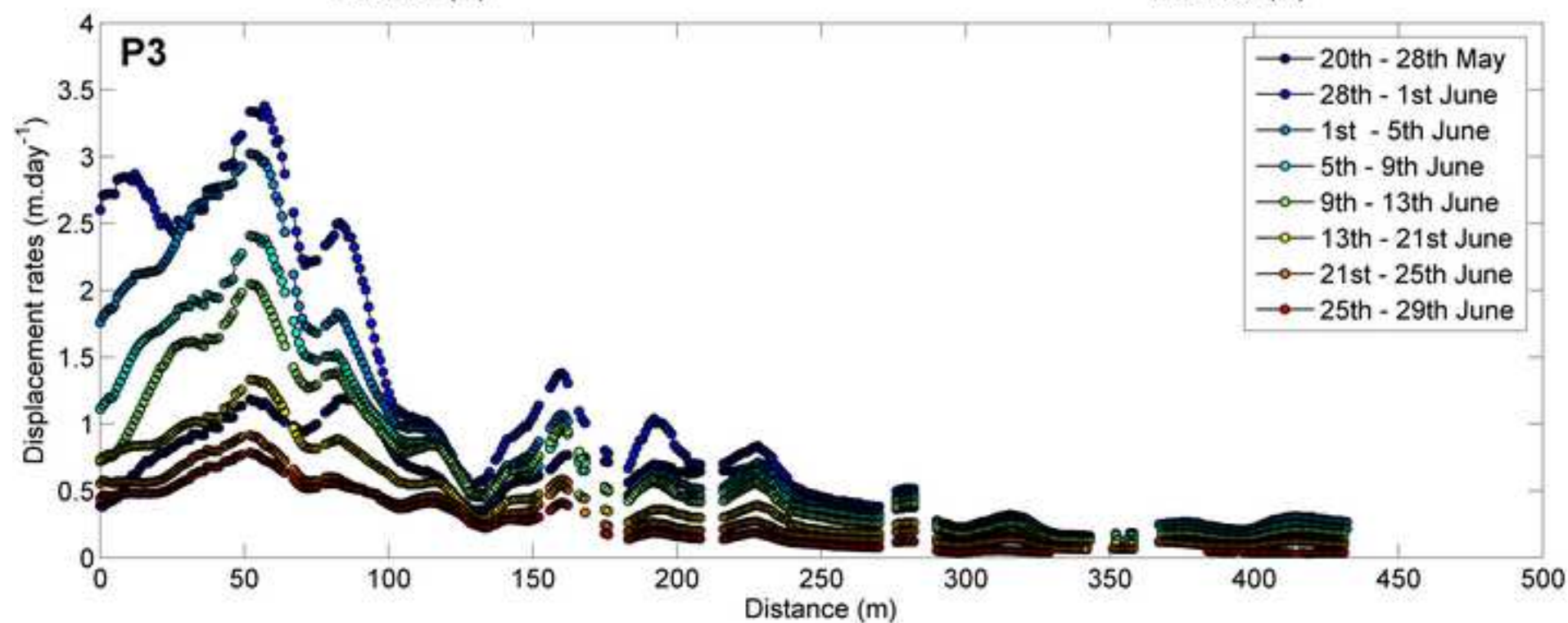
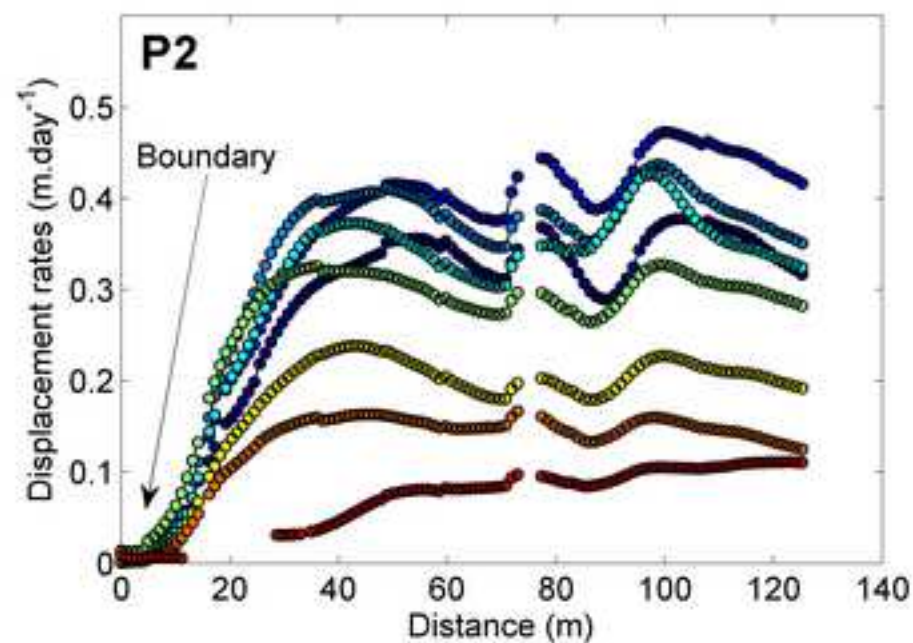
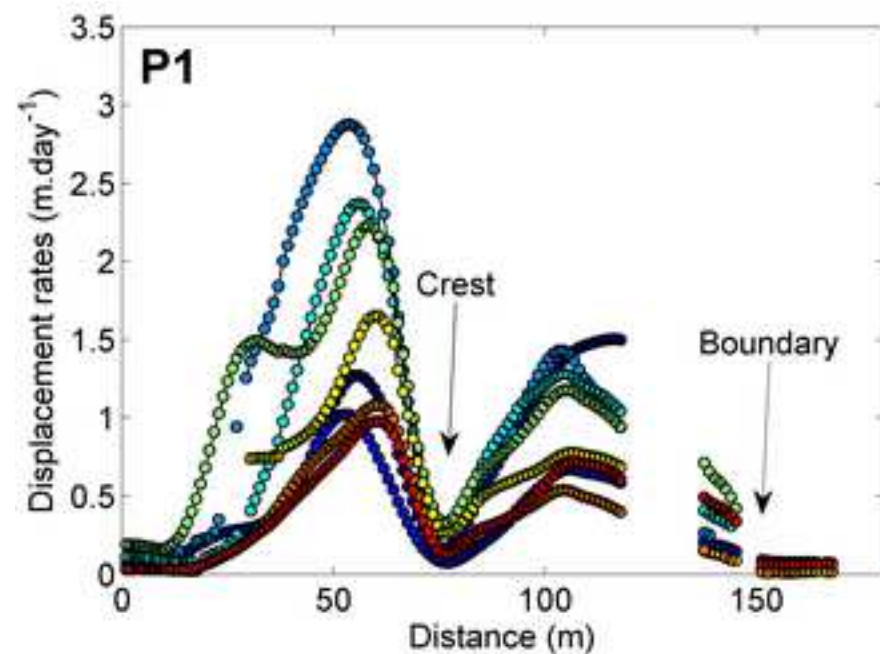


Figure(s)  
[Click here to download high resolution image](#)



Figure(s)

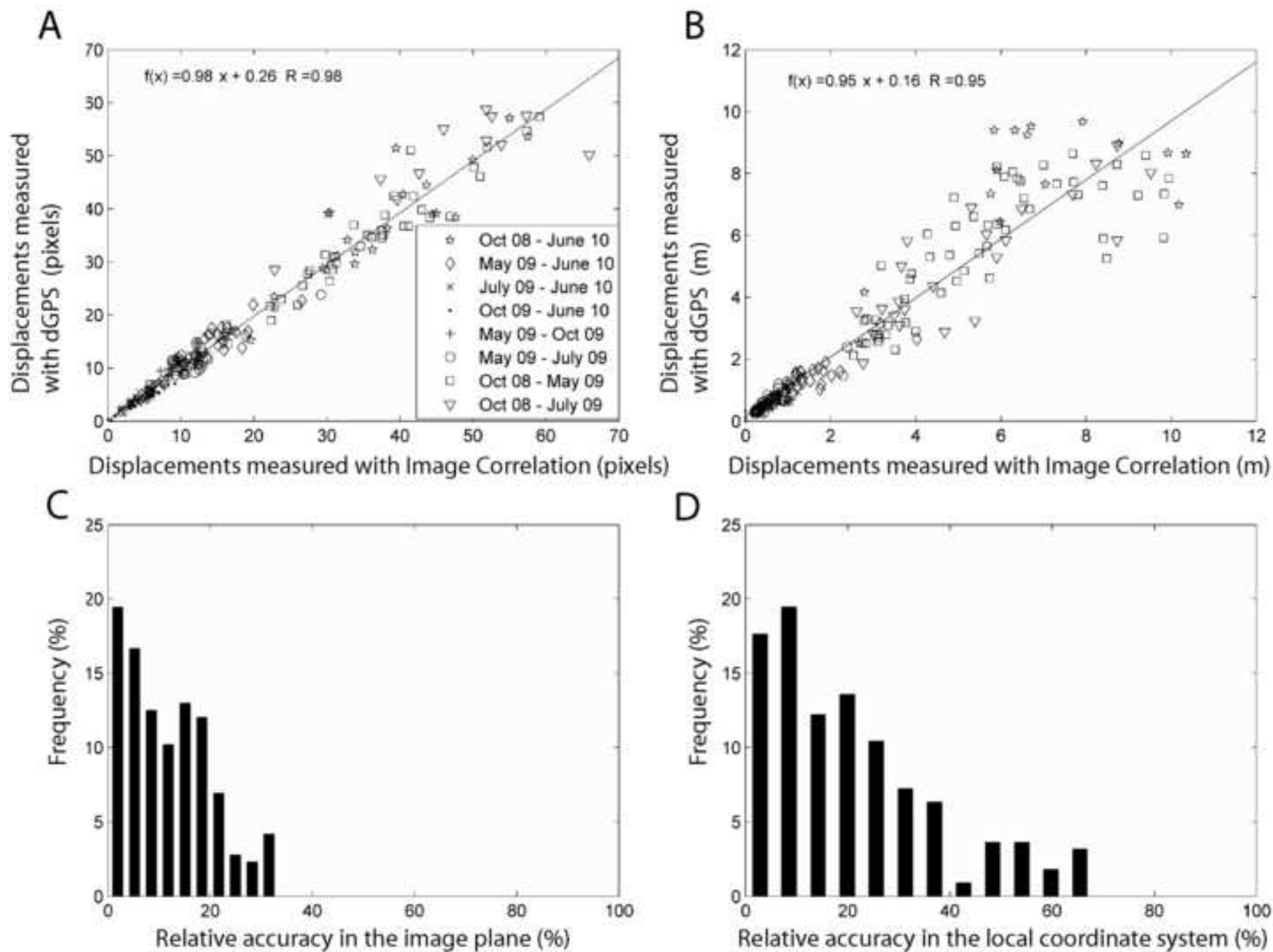
[Click here to download high resolution image](#)



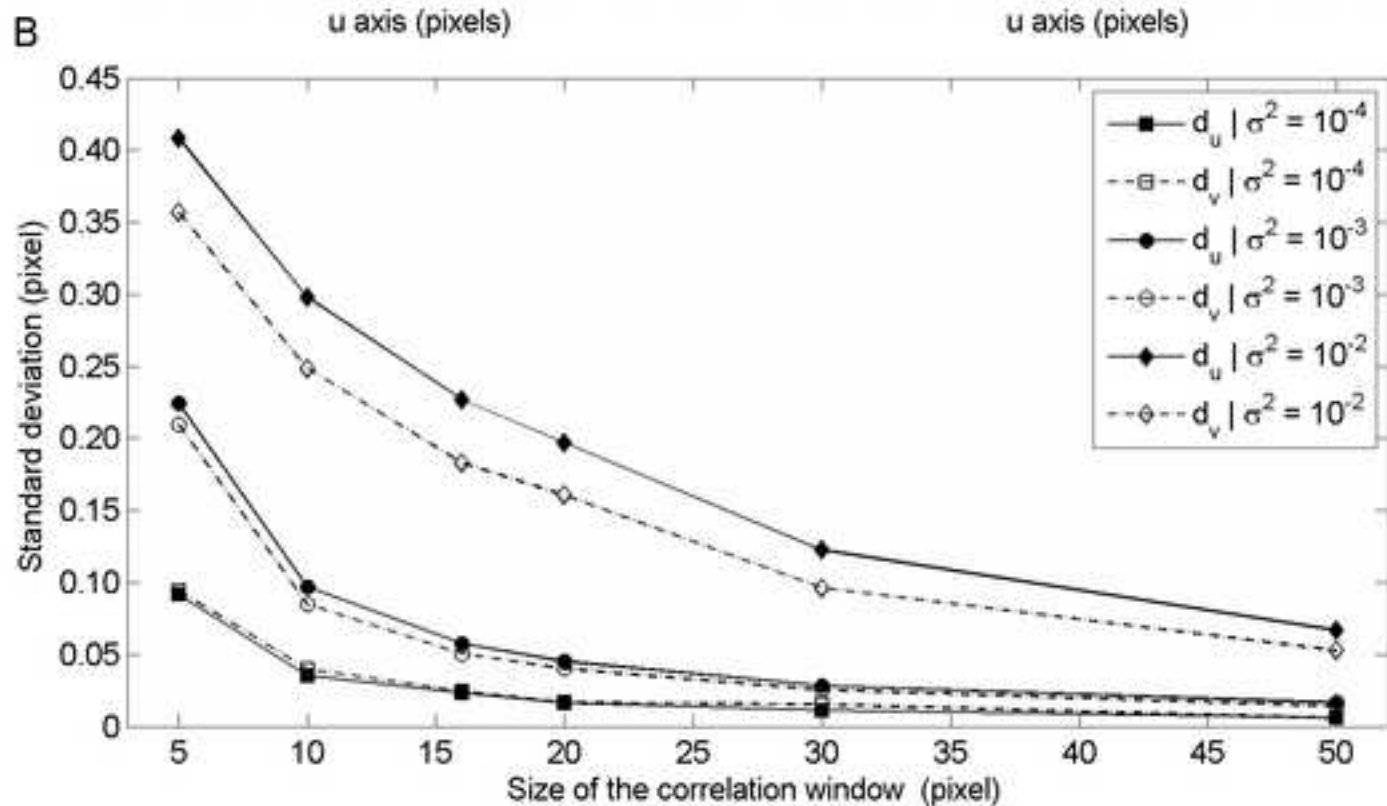
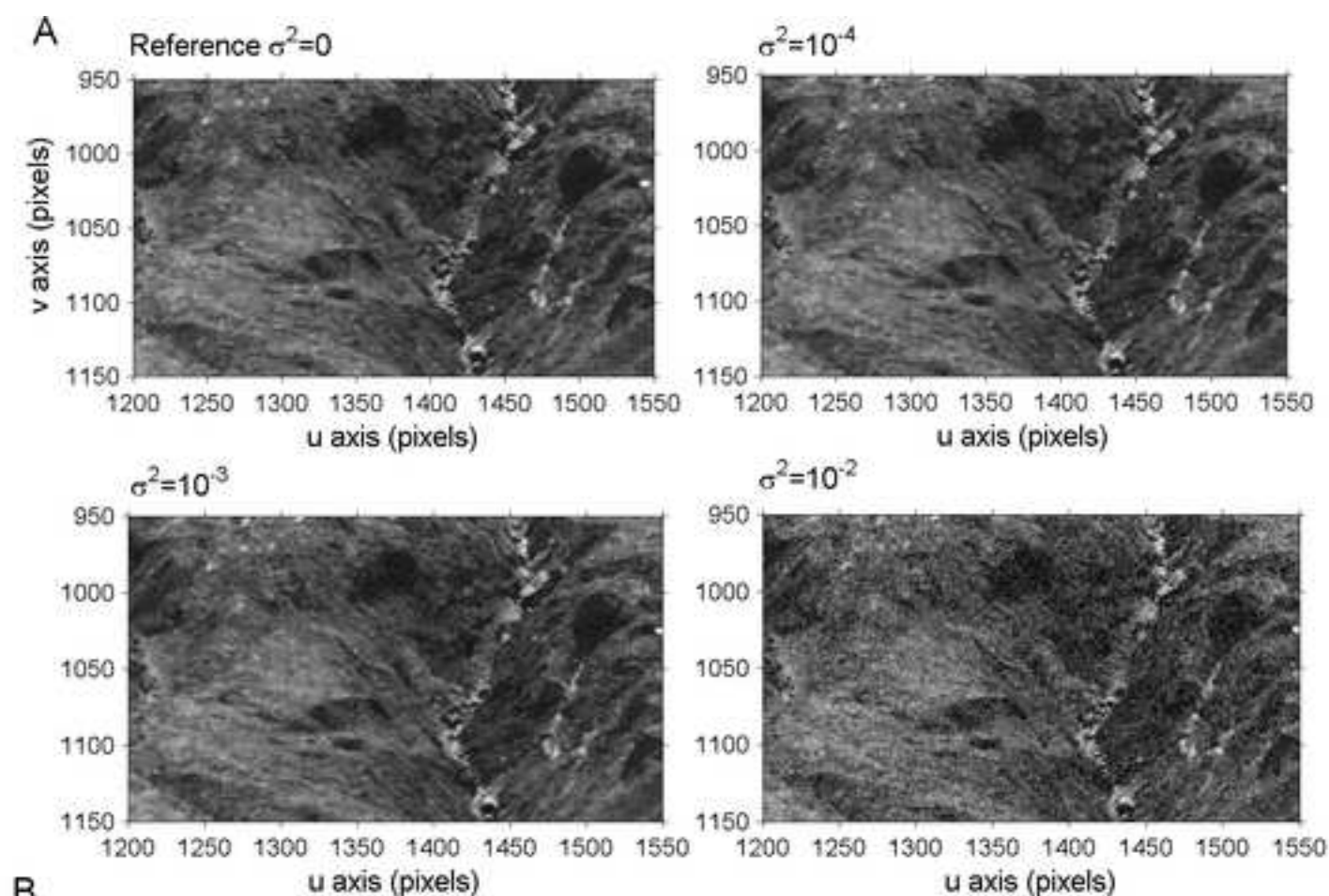


Figure(s)

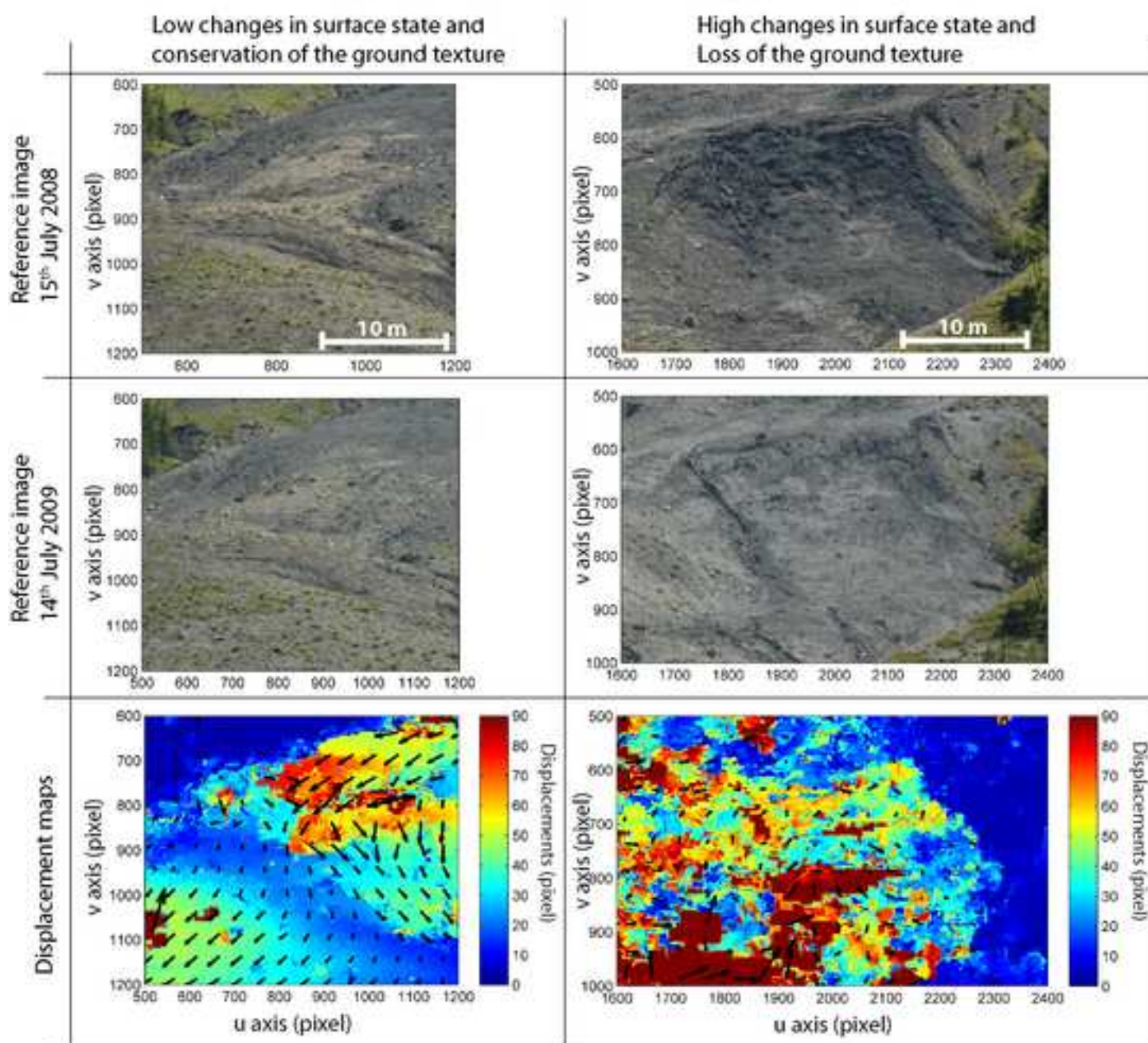
[Click here to download high resolution image](#)



Figure(s)  
[Click here to download high resolution image](#)



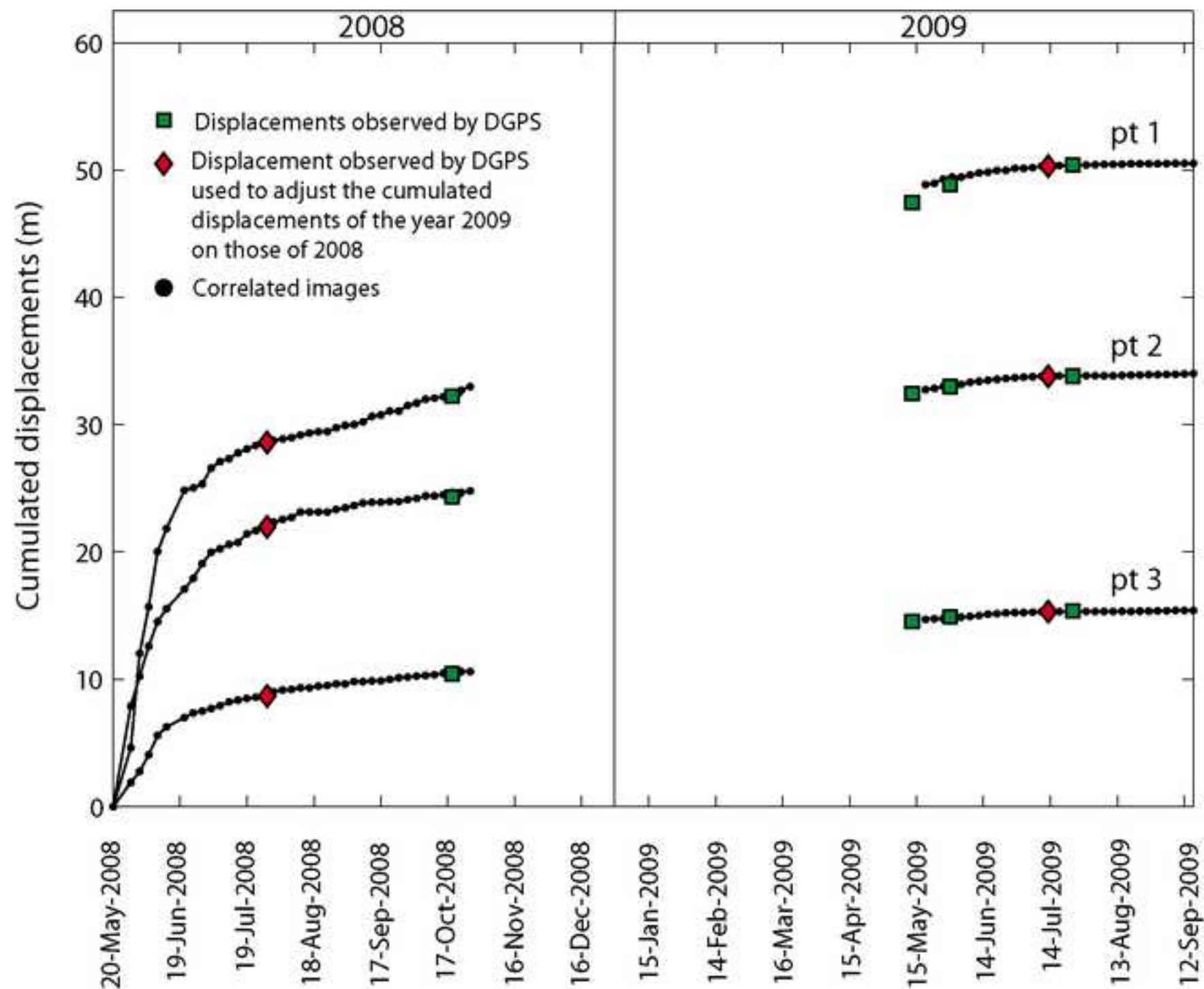
Figure(s)  
[Click here to download high resolution image](#)



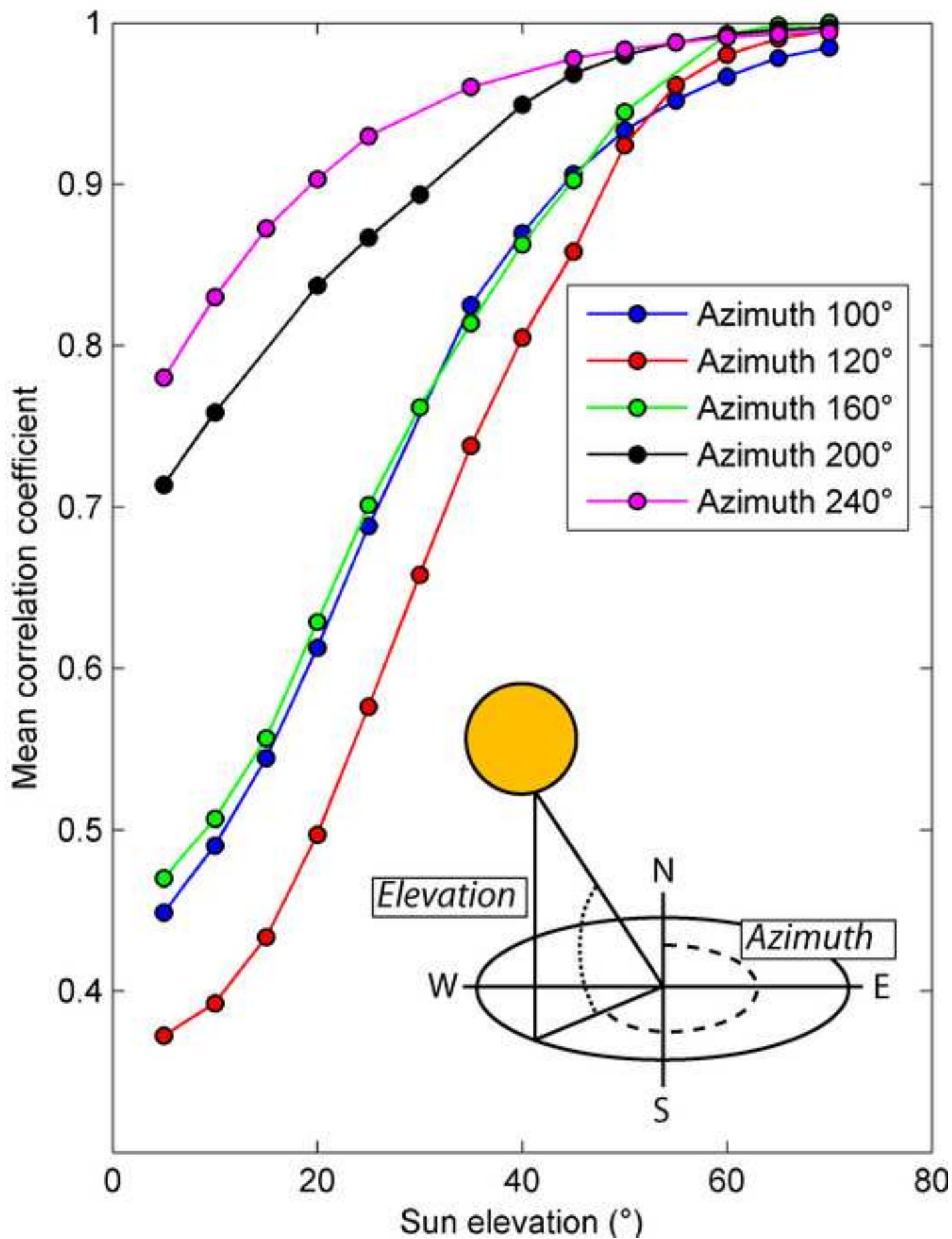


Figure(s)

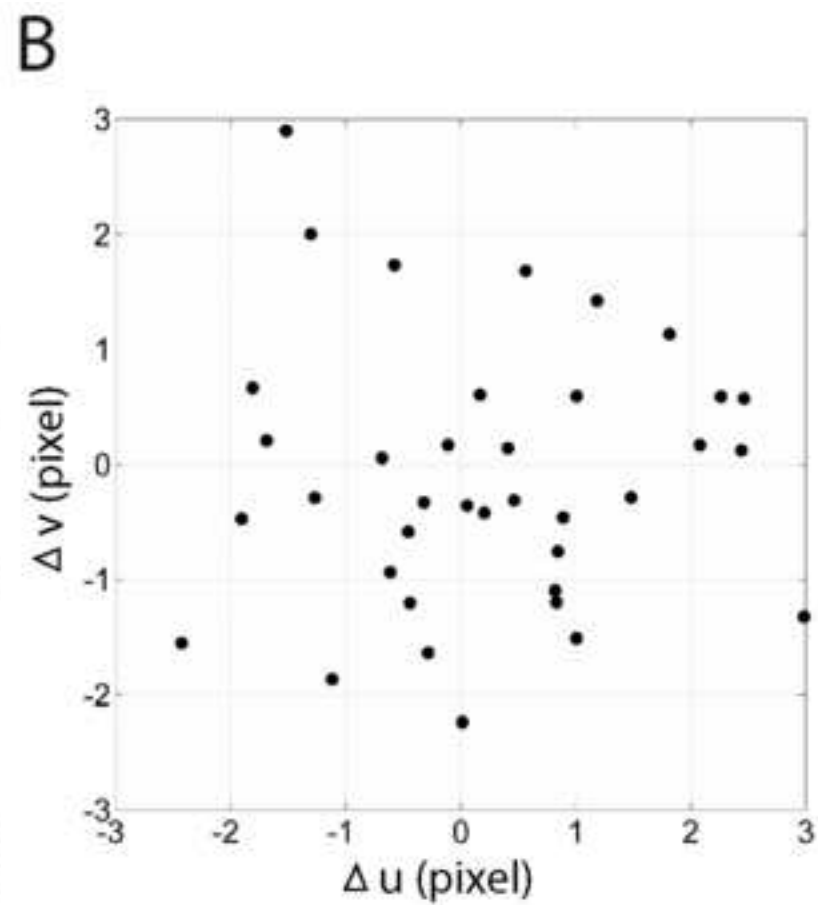
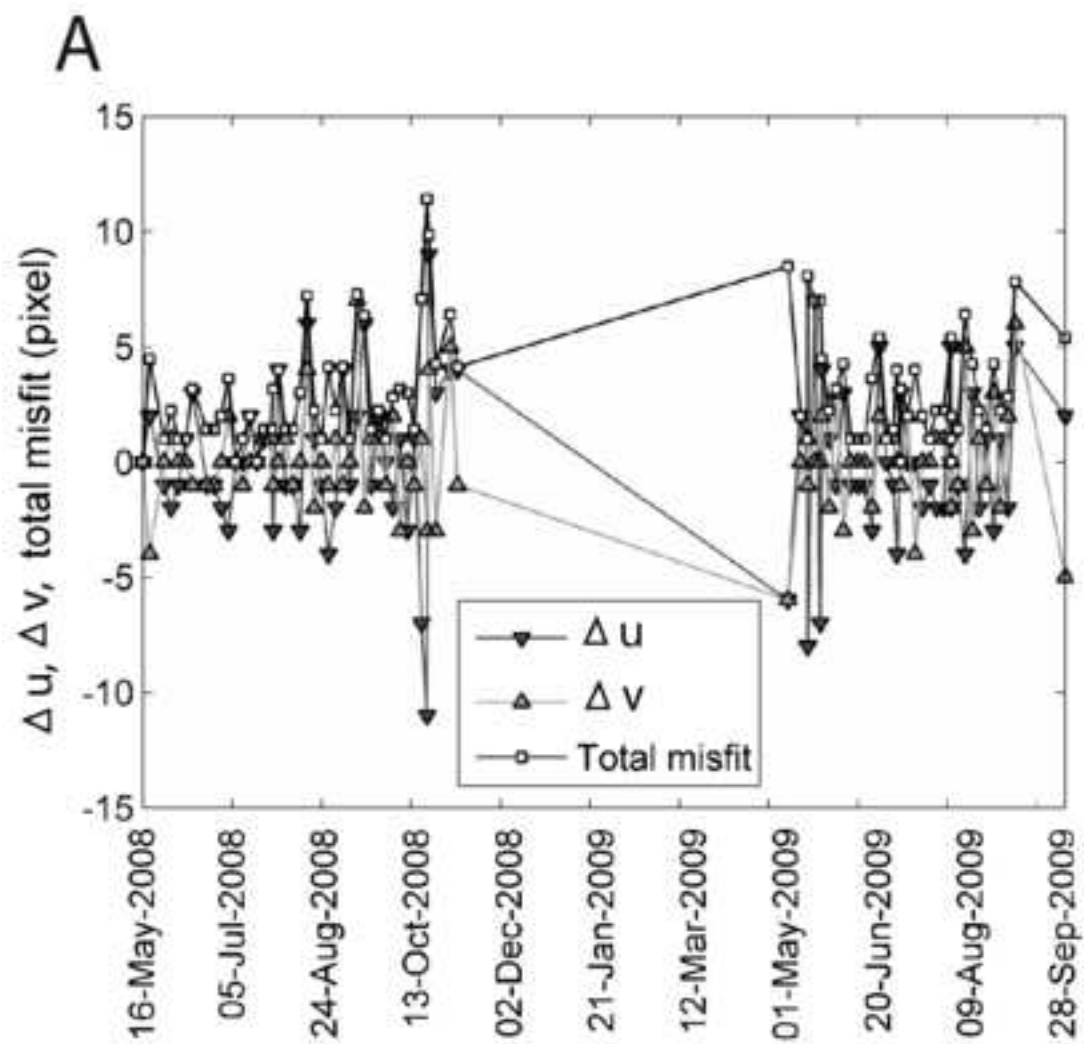
[Click here to download high resolution image](#)



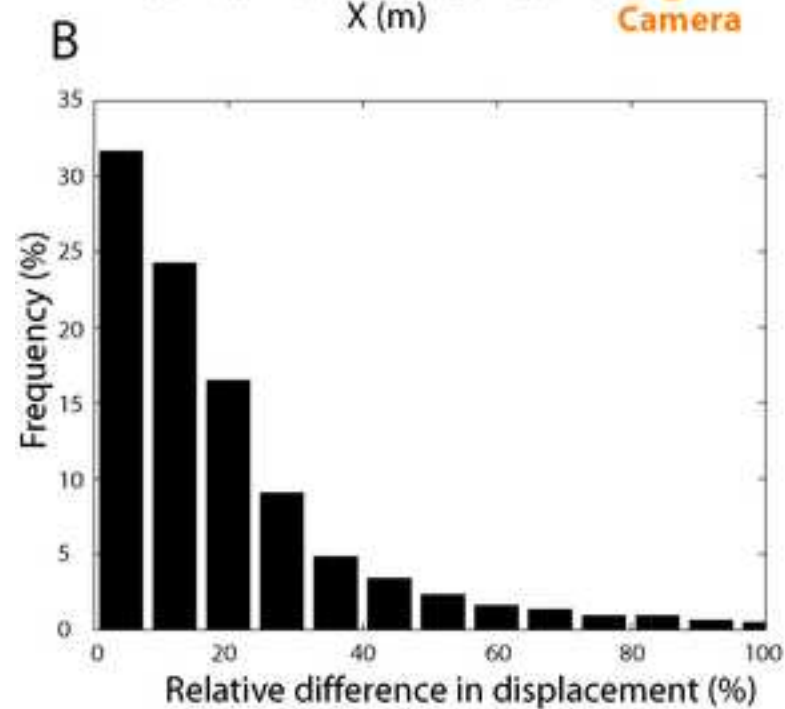
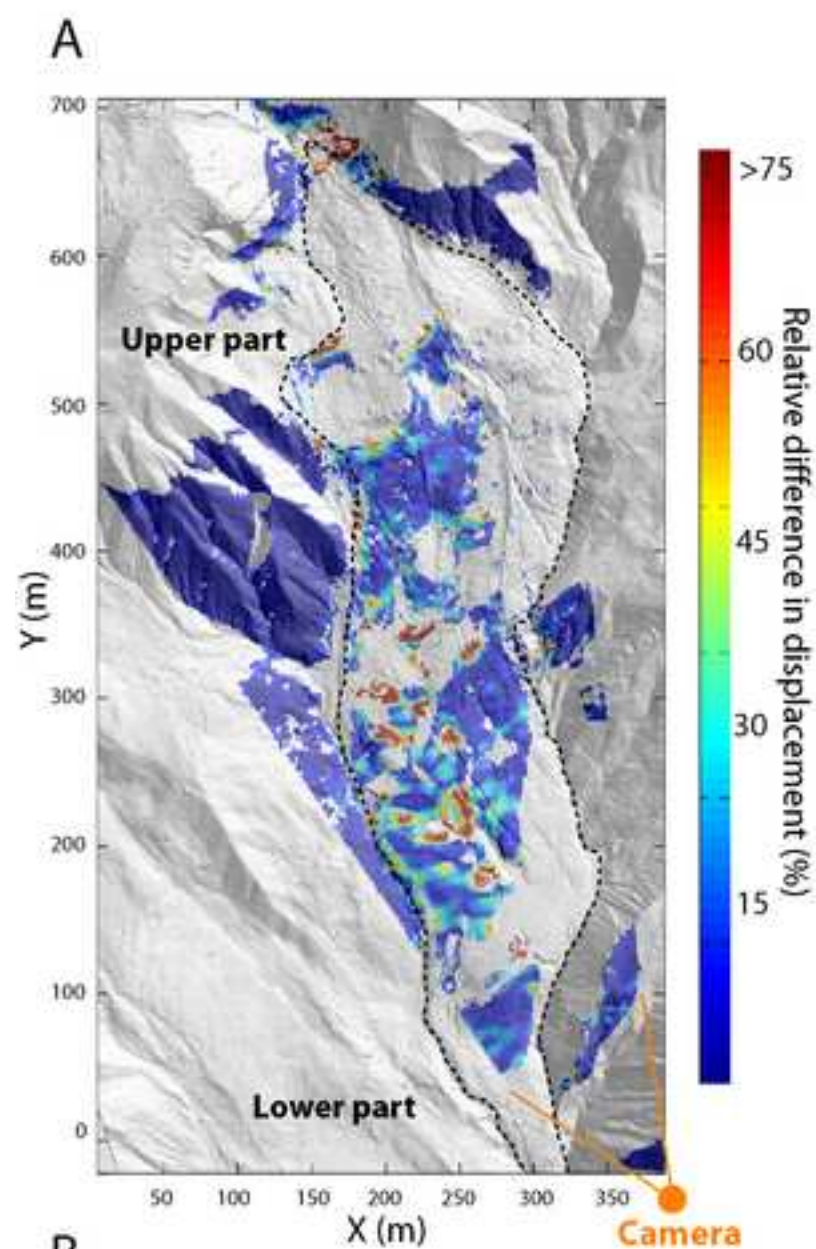
Figure(s)  
[Click here to download high resolution image](#)



Figure(s)  
[Click here to download high resolution image](#)







## Tables

Table 1. Relative advantages and disadvantages of GB-InSAR, TLS and TOP for landslide monitoring.

Techniques	Relative advantages	Relative disadvantages
GB-InSAR	High data accuracy possible (millimetric accuracy)	Requires large initial investment if buying
	Monitoring during night and any type of weather conditions	Skilled crew required for operation
	Atmospheric effects can be corrected (permanent scatterers)	Displacement along line of sight
	Potential for high level of automation in acquisition and post-processing	Fails in detecting large and rapid displacements (signal decorrelation) Sensitive to changes in acquisition geometry and surface state variations
TLS	High data accuracy possible 1-4 cm (at 100 m range); 30 cm (at 1000 m range)	Requires large initial investment if buying
	Provide an easily understandable image	Skilled crew required for operation
	Potential for high level of automation in acquisition	Computation of the true 3D displacements require specific algorithms optimized for calculations on large 3D point clouds Large amount of computational resources for the spatial data visualization Automated data post-processing difficult
TOP	High data accuracy possible from millimeters to a few centimeters at 100 m range	Adverse weather and illumination changes affects image quality
	Provide an easily understandable image	Not operating during the night
	Low initial cost and operating cost	Very Sensitive to changes in acquisition geometry and surface state variations
	Low energy supply (passive sensors)	Ortho-rectification using accurate DEM is necessary for quantitative analysis
	Potential for high level of automation in acquisition and post-processing	Ground control points necessary for camera calibration
	Simple camera calibration	
	Simple matching algorithms available to produce DEMs and to compute 2D displacement fields	

Table 2. Characteristics of the camera acquisition systems

Type of Camera	Single-lens reflex Nikon digital camera
Effective Pixels	6.1 million
Image Sensor	RGB CCD, 23.7 x 15.6 mm
Image Size	3008 x 2000 pixels
Sensitivity	400 iso
Focal length	52 mm
Shutter speed	1/800
Storage Media	CompactFlash™ (CF) Card
Storage System	NEF (Nikon RAW)

Table 3. Quantity of interpretable displacement values in summer and in autumn after filtering according to the location in the landslide (Fig. 2)

	Total		1. Correlation coefficient > 0.6		2. Downslope displacements		3. Displacements in visible areas	
	Absolute quantity of values (-)	Relative quantity of values (%)	Absolute quantity of values (-)	Relative quantity of values (%)	Absolute quantity of values (-)	Relative quantity of values (%)	Absolute quantity of values (-)	Relative quantity of values (%)
<b>23 July - 27 July 2008</b>								
Upper part	210637	100	197139	93.6	164275	78.0	161221	76.5
Middle part	24821	100	23612	95.1	23266	93.7	22343	90.0
Lower part	61979	100	61255	98.8	59989	96.8	57801	93.3
Whole landslide	297437	100	282006	94.8	247530	83.2	241365	81.1
<b>19 Oct. - 23 Oct. 2008</b>								
Upper part	210637	100	183570	87.2	82149	39.0	74798	35.5
Middle part	24821	100	22847	92.1	20751	83.6	18672	75.2
Lower part	61979	100	61762	99.7	60019	96.8	57510	92.8
Whole landslide	297437	100	268179	90.2	162919	60.4	150980	50.8

Table 4. Mean value ( $\mu$ ) and standard deviation ( $\sigma$ ) of the absolute accuracy for the projection in the image plane and the back-projection in the local coordinate system. n is the number of GCPs used for the calculation of the accuracy

Image plane (n=40)	$\mu$ (pixel)	$\sigma$ (pixel)
u	0.20	1.59
v	-0.08	1.51
Local coordinate system		
(n=11)	$\mu$ (m)	$\sigma$ (m)
X	0.07	0.41
Y	-0.13	0.53
Z	0.01	0.29